

APPENDIX 3.5-L

Results of Consolidated Undrained Triaxial  
Compression and Direct Shear Testing, STS  
Consultants Ltd., 1988



STS Consultants Ltd.  
Consulting Engineers

Laboratory Testing

Kenicott Geotechnical Project

Foth & VanDyke

REPORT



**STS Consultants Ltd.**  
 Consulting Engineers  
 111 Pfingsten Road  
 Northbrook, Illinois 60062  
 (312) 272-6520

March 15, 1988

Mr. Robert Rouse  
 Foth & VanDyke  
 2737 South Ridge Road  
 PO Box 19012  
 Green Bay, WI 54307-9012

RE: Laboratory Testing Pertaining to the Kenicott Geotechnical Project -- STS Project No. 25331

Dear Mr. Rouse:

Please find enclosed three (3) copies of laboratory test results pertaining to the above referenced testing program.

Included in our report is a discussion of the scope of services provided by STS Consultants, a description of the laboratory test equipment and testing procedures utilized throughout the testing program, a discussion of the laboratory testing results and a summarization of all laboratory testing data including graphs where applicable.

We are pleased to have been of service to you on this particular project. Should you have any questions or comments pertaining to the laboratory test data presented, the contents of this report, or if we may be of further assistance to you in any other way, please do not hesitate to contact us.

Respectfully,

STS CONSULTANTS, LTD.

*William P. Quinn*  
 William P. Quinn  
 Laboratory Manager

*Charles W. Pfingsten*  
 Charles W. Pfingsten, P.E.  
 Senior Principal Engineer

WPQ/nt  
 enc.

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Scope of Services

STS Consultants was to provide Foth & Van Dyke with laboratory test data obtained by the performance of consolidated undrained triaxial compression and direct shear tests. The tests were performed on samples delivered to our Northbrook testing facility on February 24, 1988. The samples were in the form of 3 inch Shelby tube samples that had been extruded prior to their delivery at the STS laboratory. All selected samples and testing pressures including consolidating stresses for triaxial tests and normal loads for direct shear tests were as instructed by Foth & Van Dyke.

Testing Procedures

The consolidated isotropically undrained triaxial tests were performed utilizing standard triaxial equipment. This equipment consists of a triaxial compression cell adapted to test 3 inch diameter shelly tube specimen, a pore pressure panel used to regulate both cell and back pressures and having a pressure transducer which monitors pore water pressures throughout the test, and a triaxial loader with load cell to provide vertical loads to shear the test specimens.

The initial phase of testing was to encase each of the specimens in a flexible rubber membrane and seal it into the triaxial chamber. Once sealed in the chamber, each specimen was backpressure saturated. This was accomplished by providing a pressure differential of 0.15 ksc (kilograms per square centimeter) between the cell pressure and the backpressure. The pressures were simultaneously and incrementally increased until saturating pressures of 4.15 ksc cell pressure and 4.00 ksc backpressure were attained. The specimen saturation was considered complete when a Skempton's pore pressure B parameter of 0.95 or greater was attained. This B parameter is the ratio of an increase in pore water pressure to a corresponding and simultaneous increase in cell confining pressure.

Once full saturation had been attained, the confining pressure was increased to a predetermined stress to provide a consolidating stress to the test specimen. The valves to the specimen were then opened and the pore fluids were allowed to collect in a calibrated burette. Volumetric measurements of the pore fluids were periodically made until full specimen consolidation had been completed. This was determined by the stabilization of the pore fluid volumetric measurements. Consolidating stresses of 0.70, 2.11 and 3.52 ksc (10, 30 and 50 psi, respectively) were utilized throughout the testing program.

Once full specimen consolidation had been attained, the final stage was to shear the test specimen in the triaxial loader. During the loading process, a strain rate of 0.100 millimeters per minute was utilized. For this phase of testing, deformation and

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pore water pressure measurements were recorded at regular time intervals. The procedures outlined previously were in general conformance with those procedures outlined in the Corps of Engineers Testing Manual EM110-2-1906, Appendix X.

The direct shear test was performed utilizing a Wykeham Farrance direct shear device. The test was performed as a consolidated drained direct shear test, utilizing one normal load per test as per instructions received from Foth & Van Dyke. A total of 3 tests were performed with normal loads of 0.7, 2.11 and 3.52 ksc (10, 30 and 50 psi). Strain rates of the tests were determined by determining the time of failure as  $50 \times T_{50}$  where  $T_{50}$  was the time required for specimen to achieve 50% of consolidation under the normal force. It is assumed that this rate of strain was sufficient to allow full drainage throughout the loading of the test specimen although the tests are normally performed utilizing 3 separate points, to eliminate assumptions.

During the setup of the direct shear specimens, a small section of the undisturbed sample was trimmed to approximately a 2 centimeter height. This was accomplished by trimming the specimen to fit into the direct shear shearing box. A normal force was then applied to the top of the test specimen and the consolidation of the specimen was recorded. During this time, water was used to fully inundate the test specimen in the shear box. When the consolidation of the test specimen had been completed, the top of the shear box was raised approximately 1/10 inch and a horizontal shearing force was applied to the shear box until the specimen was completely sheared. During this time, horizontal load, horizontal and vertical deformation readings were recorded. The test was performed in general conformance with those procedures outlined in ASTM D-3080, "Direct Shear Test of Soils Under Consolidated Drained Conditions".

#### Laboratory Test Results

The samples delivered to the STS laboratory for testing consisted of mostly silt material. Three of the four triaxial tests consisted of 3 separate points. The test utilizing specimens labeled S5, 45-47 feet consisted of two specimens. A third specimen originally scheduled for testing consisted mostly of sand. We were unable to obtain a suitable specimen for testing. The condition of all the specimens indicated some sample disturbance by the gouges on the specimen sides. Also moisture content and dry density test results varied from 1 to 2 percent, with samples used for the same triaxial test.

The direct shear test performed on S4, 31.5 to 32.5 feet indicates a very high shear stress. The sample initially was very dense and slightly dessicated. We recommend additional direct shear points be performed to determine a  $\phi$  angle passing through the origin.

A summarization of all laboratory testing including graphs where applicable is attached to this report.



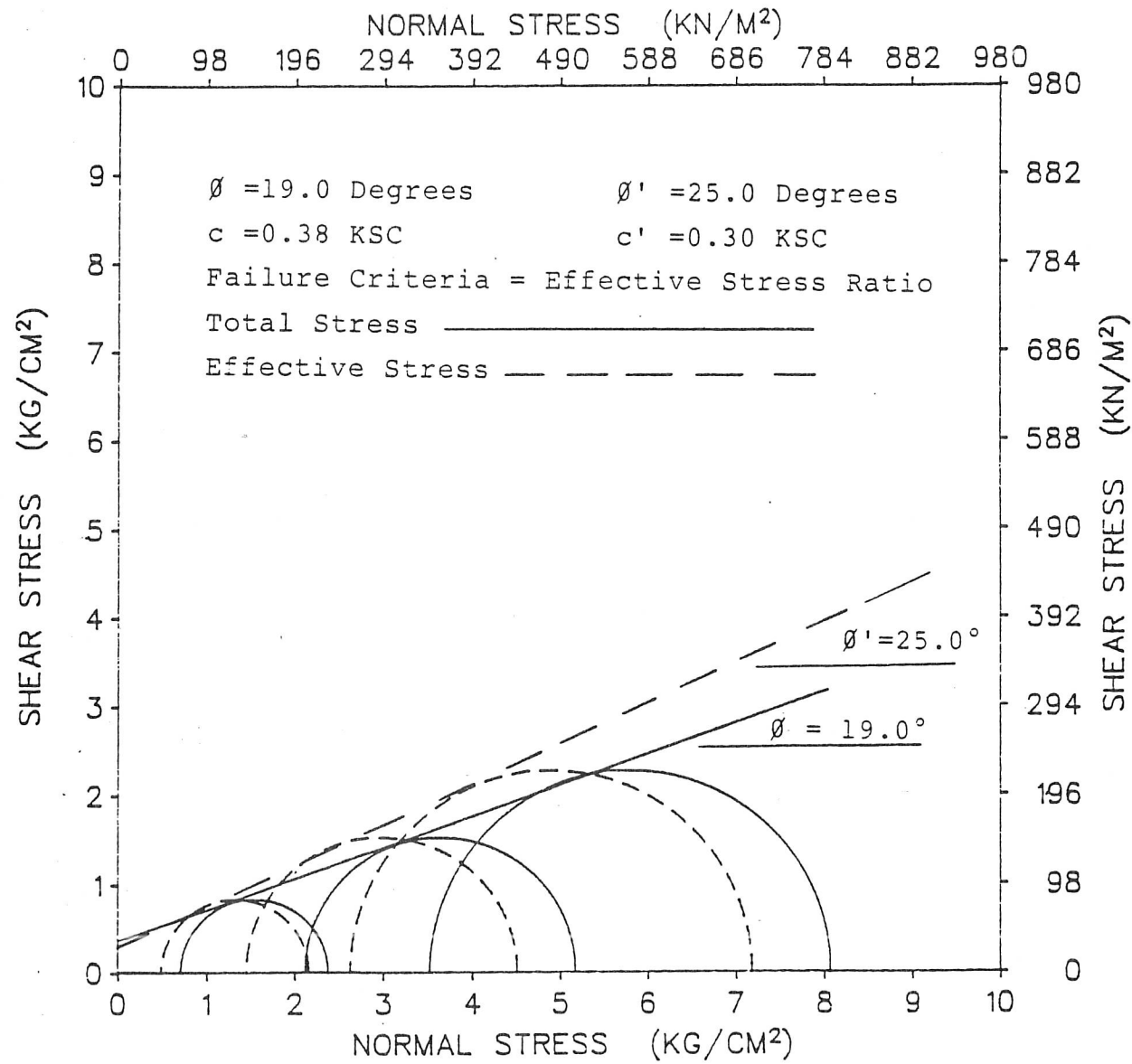
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|         |             |              |
|---------|-------------|--------------|
| Boring: | Sample: S-1 | Depth: 25-27 |
| Boring: | Sample: S-1 | Depth: 27-29 |
| Boring: | Sample: S-1 | Depth: 23-25 |

MOHR ENVELOPE



Sigma 3 = 0.7 ksc  
 Sigma 3 = 2.1 ksc  
 Sigma 3 = 3.5 ksc

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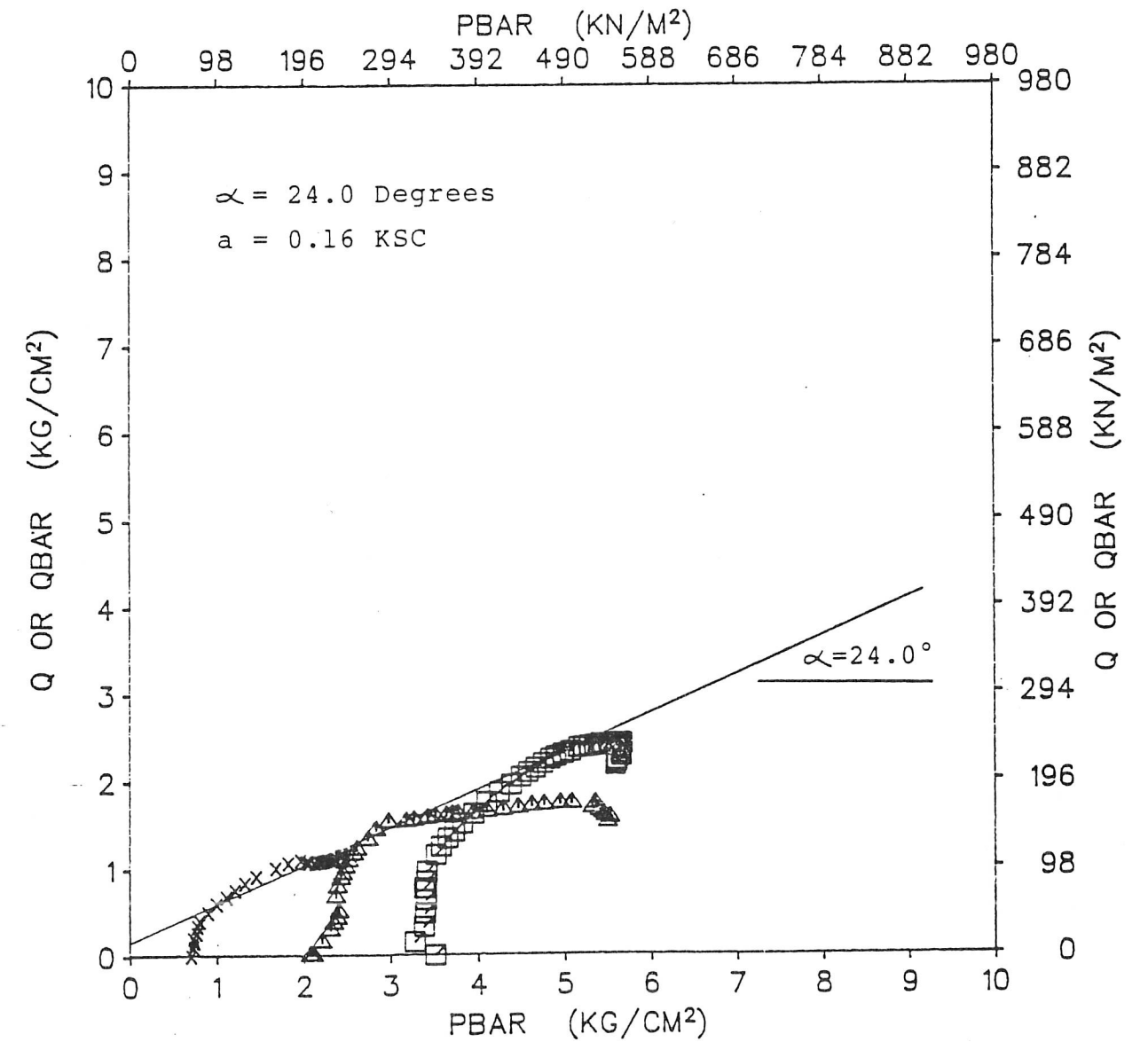
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|         |             |              |
|---------|-------------|--------------|
| Boring: | Sample: S-1 | Depth: 25-27 |
| Boring: | Sample: S-1 | Depth: 27-29 |
| Boring: | Sample: S-1 | Depth: 23-25 |

STRESS PATH PLOT



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.1 ksc  
 □ Sigma 3 = 3.5 ksc

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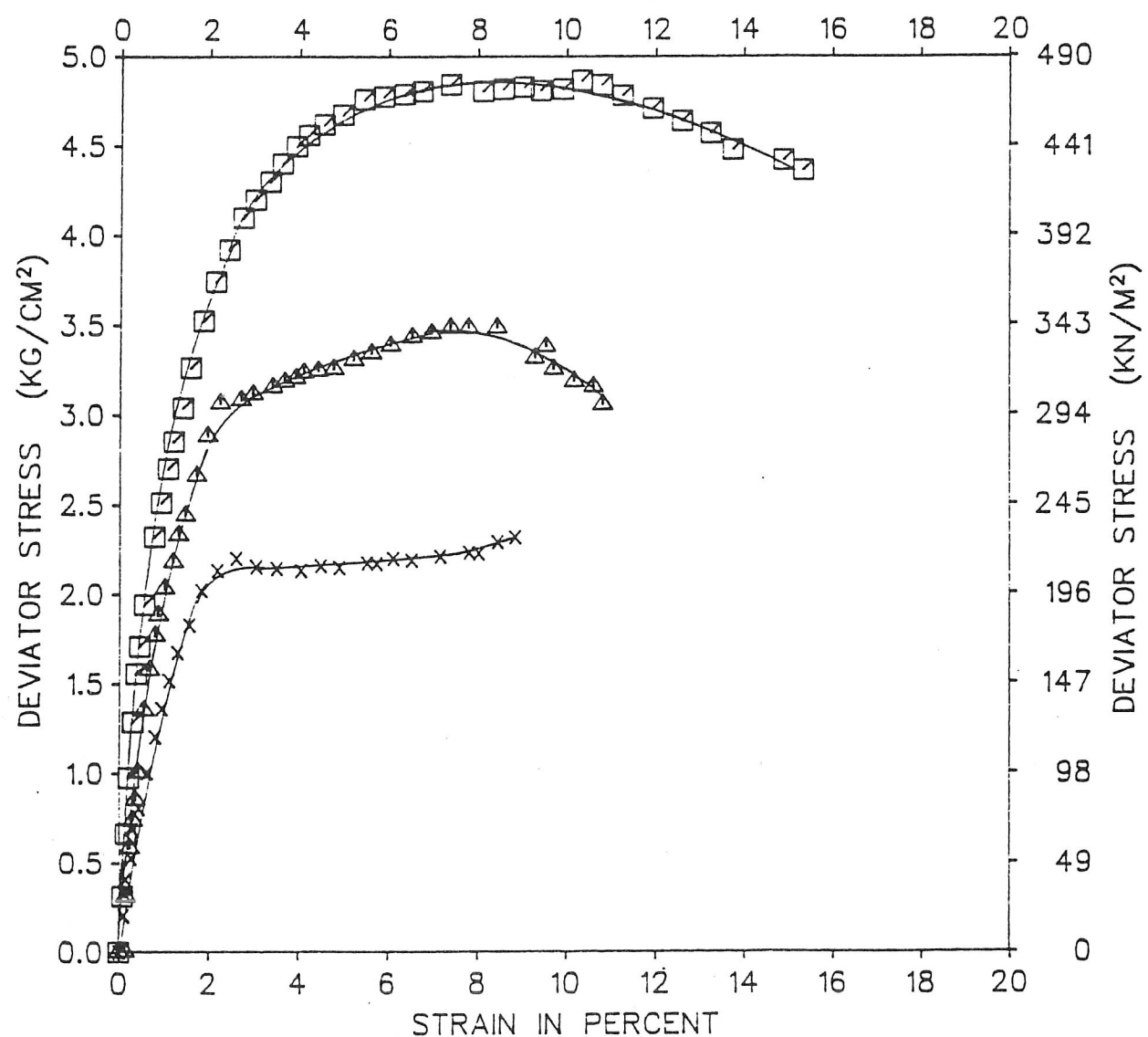
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|         |             |              |
|---------|-------------|--------------|
| Boring: | Sample: S-1 | Depth: 25-27 |
| Boring: | Sample: S-1 | Depth: 27-29 |
| Boring: | Sample: S-1 | Depth: 23-25 |

DEVIATOR STRESS vs STRAIN



- x  $\sigma_3 = 0.7$  ksc
- △  $\sigma_3 = 2.1$  ksc
- $\sigma_3 = 3.5$  ksc

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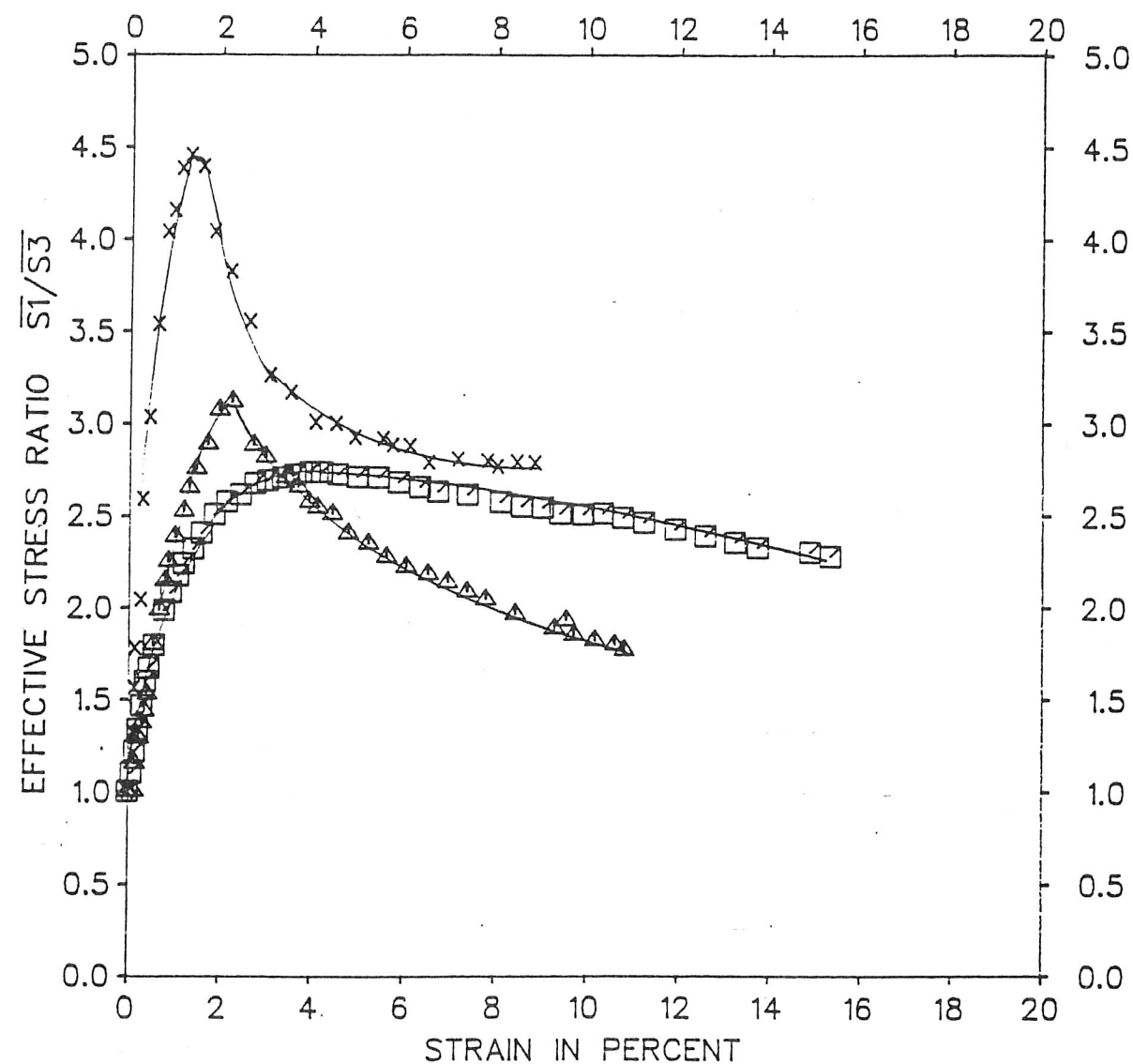
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|         |             |              |
|---------|-------------|--------------|
| Boring: | Sample: S-1 | Depth: 25-27 |
| Boring: | Sample: S-1 | Depth: 27-29 |
| Boring: | Sample: S-1 | Depth: 23-25 |

EFFECTIVE STRESS RATIO vs STRAIN



- x  $\sigma_3 = 0.7$  ksc
- △  $\sigma_3 = 2.1$  ksc
- $\sigma_3 = 3.5$  ksc

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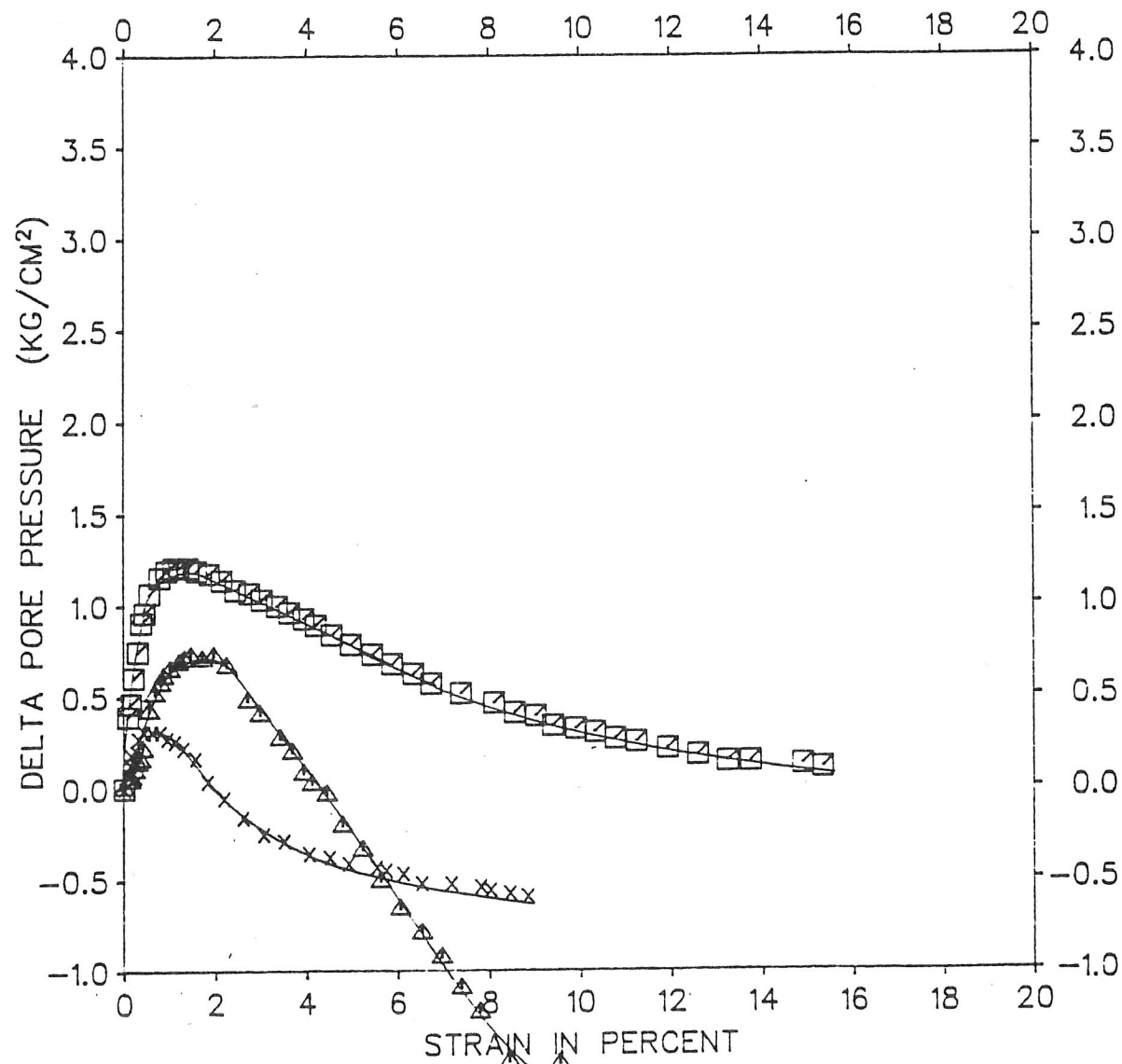
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|         |             |              |
|---------|-------------|--------------|
| Boring: | Sample: S-1 | Depth: 25-27 |
| Boring: | Sample: S-1 | Depth: 27-29 |
| Boring: | Sample: S-1 | Depth: 23-25 |

DELTA PORE PRESSURE vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.1 ksc  
 □ Sigma 3 = 3.5 ksc

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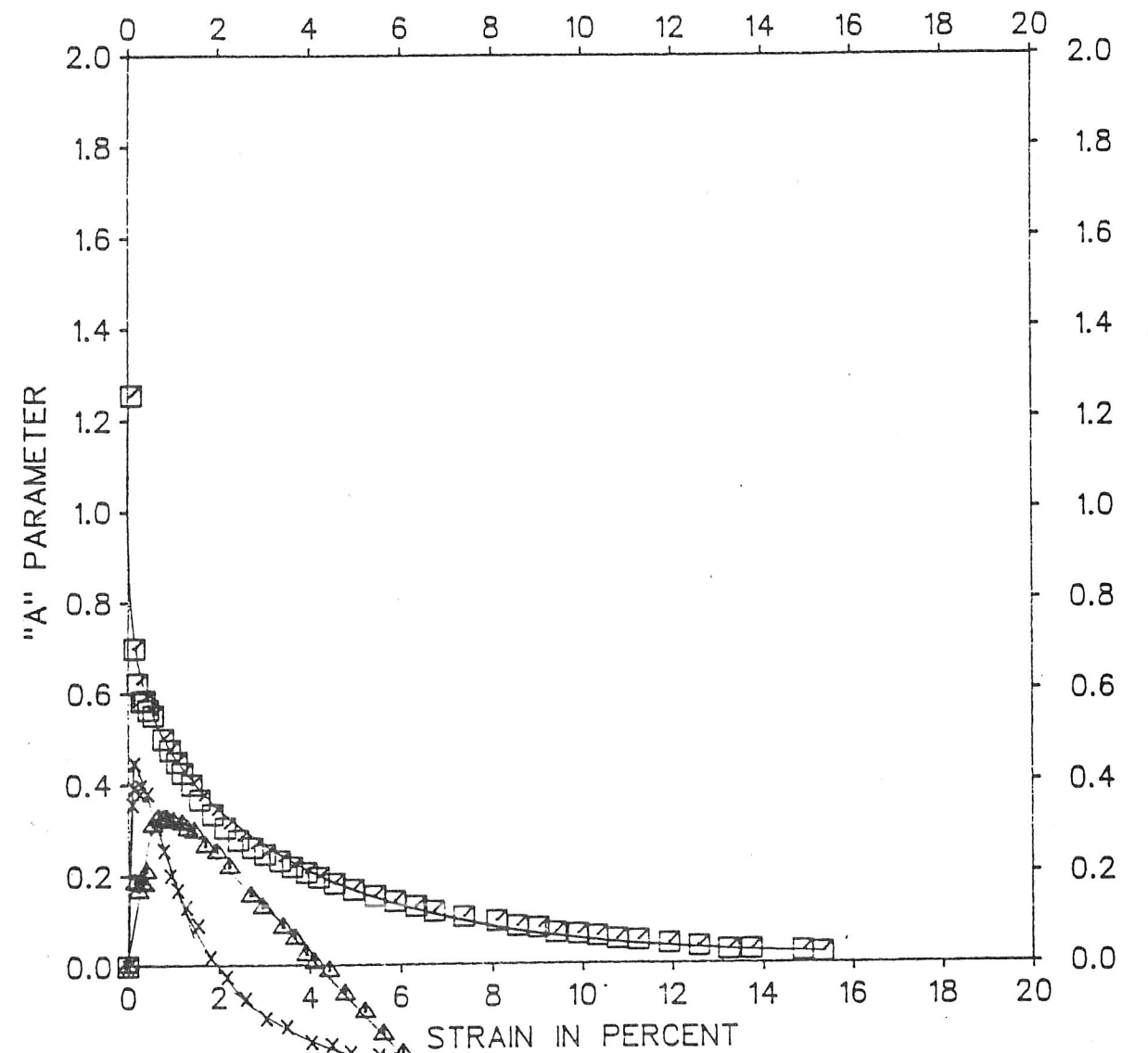
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|         |             |              |
|---------|-------------|--------------|
| Boring: | Sample: S-1 | Depth: 25-27 |
| Boring: | Sample: S-1 | Depth: 27-29 |
| Boring: | Sample: S-1 | Depth: 23-25 |

"A" PARAMETER vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.1 ksc  
 □ Sigma 3 = 3.5 ksc

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BORING:  
 SAMPLE: S-1  
 DEPTH: 25-27

STS JOB NO: 25331  
 EFF. SIGMA3: 0.700 KG/CM2

TEST RESULTS-----

| LOAD | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P     | PBAR   | Q OR   | A      |
|------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|
| KG   | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | KG/CM2 | S3     | S3BAR | KG/CM2 | KG/CM2 | KG/CM2 |
| 0.0  | 0.00  | 3800. | 0.00   | 0.70   | 0.70   | 0.70   | 0.70   | 0.0    | 0.00   | 1.00   | 0.70  | 0.70   | 0.00   | 0.00   |
| 7.7  | 0.16  | 3804. | 0.07   | 0.90   | 0.70   | 0.83   | 0.63   | 0.1    | 0.20   | 1.32   | 0.80  | 0.73   | 0.10   | 0.36   |
| 12.3 | 0.20  | 3805. | 0.13   | 1.02   | 0.70   | 0.90   | 0.57   | 0.1    | 0.32   | 1.56   | 0.86  | 0.74   | 0.16   | 0.39   |
| 15.4 | 0.22  | 3805. | 0.18   | 1.10   | 0.70   | 0.92   | 0.52   | 0.1    | 0.40   | 1.78   | 0.90  | 0.72   | 0.20   | 0.44   |
| 20.0 | 0.40  | 3810. | 0.20   | 1.22   | 0.70   | 1.03   | 0.50   | 0.3    | 0.52   | 2.04   | 0.96  | 0.76   | 0.26   | 0.38   |
| 26.1 | 0.44  | 3811. | 0.27   | 1.38   | 0.70   | 1.11   | 0.43   | 0.3    | 0.68   | 2.59   | 1.04  | 0.77   | 0.34   | 0.39   |
| 30.7 | 0.66  | 3817. | 0.30   | 1.50   | 0.70   | 1.20   | 0.39   | 0.4    | 0.80   | 3.04   | 1.10  | 0.80   | 0.40   | 0.38   |
| 38.3 | 0.92  | 3823. | 0.30   | 1.70   | 0.70   | 1.40   | 0.39   | 0.6    | 1.00   | 3.54   | 1.20  | 0.90   | 0.50   | 0.30   |
| 46.0 | 1.19  | 3830. | 0.30   | 1.90   | 0.70   | 1.60   | 0.39   | 0.8    | 1.20   | 4.04   | 1.30  | 1.00   | 0.60   | 0.25   |
| 52.1 | 1.41  | 3836. | 0.27   | 2.06   | 0.70   | 1.79   | 0.43   | 0.9    | 1.36   | 4.16   | 1.38  | 1.11   | 0.68   | 0.20   |
| 58.3 | 1.65  | 3842. | 0.25   | 2.22   | 0.70   | 1.96   | 0.45   | 1.1    | 1.52   | 4.38   | 1.46  | 1.21   | 0.76   | 0.17   |
| 64.4 | 1.93  | 3850. | 0.22   | 2.37   | 0.70   | 2.16   | 0.48   | 1.3    | 1.67   | 4.46   | 1.54  | 1.32   | 0.84   | 0.13   |
| 70.5 | 2.33  | 3860. | 0.16   | 2.53   | 0.70   | 2.36   | 0.54   | 1.6    | 1.83   | 4.39   | 1.61  | 1.45   | 0.91   | 0.09   |
| 78.2 | 2.73  | 3871. | 0.04   | 2.72   | 0.70   | 2.68   | 0.66   | 1.8    | 2.02   | 4.04   | 1.71  | 1.67   | 1.01   | 0.02   |
| 82.8 | 3.27  | 3885. | -0.05  | 2.83   | 0.70   | 2.89   | 0.75   | 2.2    | 2.13   | 3.83   | 1.77  | 1.82   | 1.07   | -0.03  |
| 85.8 | 3.90  | 3902. | -0.16  | 2.90   | 0.70   | 3.06   | 0.86   | 2.6    | 2.20   | 3.55   | 1.90  | 1.96   | 1.10   | -0.07  |
| 84.3 | 4.56  | 3920. | -0.25  | 2.85   | 0.70   | 3.10   | 0.95   | 3.1    | 2.15   | 3.26   | 1.78  | 2.03   | 1.08   | -0.12  |
| 84.3 | 5.24  | 3938. | -0.29  | 2.84   | 0.70   | 3.13   | 0.99   | 3.5    | 2.14   | 3.17   | 1.77  | 2.06   | 1.07   | -0.13  |
| 84.3 | 6.05  | 3960. | -0.36  | 2.83   | 0.70   | 3.19   | 1.06   | 4.1    | 2.13   | 3.01   | 1.76  | 2.12   | 1.06   | -0.17  |
| 85.8 | 6.71  | 3979. | -0.38  | 2.86   | 0.70   | 3.23   | 1.08   | 4.5    | 2.16   | 3.00   | 1.78  | 2.16   | 1.08   | -0.17  |
| 85.8 | 7.33  | 3996. | -0.41  | 2.85   | 0.70   | 3.26   | 1.11   | 4.9    | 2.15   | 2.93   | 1.77  | 2.19   | 1.07   | -0.19  |
| 87.4 | 8.25  | 4022. | -0.43  | 2.87   | 0.70   | 3.30   | 1.13   | 5.5    | 2.17   | 2.92   | 1.79  | 2.22   | 1.09   | -0.20  |
| 87.4 | 8.56  | 4031. | -0.45  | 2.87   | 0.70   | 3.32   | 1.15   | 5.7    | 2.17   | 2.89   | 1.78  | 2.23   | 1.08   | -0.21  |
| 88.9 | 9.12  | 4047. | -0.47  | 2.90   | 0.70   | 3.36   | 1.17   | 6.1    | 2.20   | 2.88   | 1.80  | 2.27   | 1.10   | -0.21  |
| 88.9 | 9.72  | 4065. | -0.52  | 2.89   | 0.70   | 3.41   | 1.22   | 6.5    | 2.19   | 2.79   | 1.79  | 2.31   | 1.09   | -0.24  |
| 90.4 | 10.68 | 4093. | -0.52  | 2.91   | 0.70   | 3.43   | 1.22   | 7.2    | 2.21   | 2.81   | 1.80  | 2.32   | 1.10   | -0.24  |
| 91.9 | 11.65 | 4122. | -0.54  | 2.93   | 0.70   | 3.47   | 1.24   | 7.8    | 2.23   | 2.80   | 1.81  | 2.35   | 1.11   | -0.24  |
| 91.9 | 11.97 | 4131. | -0.56  | 2.92   | 0.70   | 3.48   | 1.26   | 8.0    | 2.22   | 2.77   | 1.81  | 2.37   | 1.11   | -0.25  |
| 95.0 | 12.61 | 4151. | -0.57  | 2.99   | 0.70   | 3.56   | 1.27   | 8.5    | 2.29   | 2.80   | 1.84  | 2.42   | 1.14   | -0.25  |
| 96.5 | 13.19 | 4168. | -0.59  | 3.01   | 0.70   | 3.61   | 1.29   | 8.8    | 2.31   | 2.79   | 1.86  | 2.45   | 1.16   | -0.26  |

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TRIAxIAL COMPRESSION TEST  
 CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
 BORING: S-1  
 SAMPLE: S-1  
 DEPTH: 27-29  
 SOIL DESC: CLAYEY SILT TRACE FINE SAND --  
 LTR. YELLOW BROWN & WHITE (ML)

STS JOB NO: 25331  
 DATE: 3-1-88  
 TESTED BY: JJ  
 APPROVED BY: JJ

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS----- |       | INITIAL | CONSOLIDATED |
|-------------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE              | MM    | 70.620  | 69.266       |
| LENGTH---AVERAGE              | MM    | 145.600 | 144.580      |
| AREA                          | CM2   | 39.169  | 37.682       |
| VOLUME                        | CM3   | 570.304 | 544.801      |
| WET DENSITY                   | G/CM3 | 2.243   | 2.395        |
| DRY DENSITY                   | G/CM3 | 2.012   | 2.106        |
| WATER CONTENT                 | %     | 11.500  | 13.700       |

| TEST PARAMETERS FOR CONSOLIDATION----- |        |       |
|--|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE           | KG/CM2 | 6.110 |
| TOTAL SIGMA3 + BACK PRESSURE           | KG/CM2 | 6.110 |
| BACK PRESSURE                          | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                      | KG/CM2 | 2.110 |
| EFFECTIVE SIGMA 3                      | KG/CM2 | 2.110 |
| CONSOLIDATION RATIO                    |        | 1.000 |
| STRAIN RATE                            | MM/MIN | 0.100 |

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BORING: S-1  
 SAMPLE: S-1  
 DEPTH: 27-29

STS JOB NO: 25331  
 EFF. SIGMA3: 2.110 KG/CM2

STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
 CONSOLIDATED UNDRAINED - DATA

TEST RESULTS

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P      | PBAR   | Q OR   | A     |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| KG    | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | KG/CM2 | S3BAR  | KG/CM2 | KG/CM2 | KG/CM2 |       |
| 0.0   | 0.00  | 3768. | 0.00   | 2.11   | 2.11   | 2.11   | 2.11   | 0.0    | 0.00   | 1.00   | 2.11   | 2.11   | 0.00   | 0.00  |
| 11.8  | 0.22  | 3774. | 0.06   | 2.42   | 2.11   | 2.36   | 2.05   | 0.2    | 0.31   | 1.15   | 2.27   | 2.21   | 0.16   | 0.18  |
| 22.0  | 0.34  | 3777. | 0.10   | 2.69   | 2.11   | 2.60   | 2.01   | 0.2    | 0.58   | 1.29   | 2.40   | 2.31   | 0.29   | 0.16  |
| 27.8  | 0.44  | 3780. | 0.13   | 2.85   | 2.11   | 2.71   | 1.98   | 0.3    | 0.74   | 1.37   | 2.48   | 2.34   | 0.37   | 0.18  |
| 32.2  | 0.52  | 3782. | 0.15   | 2.96   | 2.11   | 2.81   | 1.96   | 0.4    | 0.85   | 1.43   | 2.54   | 2.38   | 0.43   | 0.18  |
| 38.0  | 0.59  | 3784. | 0.21   | 3.11   | 2.11   | 2.91   | 1.90   | 0.4    | 1.00   | 1.53   | 2.61   | 2.40   | 0.50   | 0.21  |
| 51.1  | 0.79  | 3789. | 0.42   | 3.46   | 2.11   | 3.04   | 1.69   | 0.5    | 1.35   | 1.80   | 2.78   | 2.37   | 0.67   | 0.31  |
| 59.8  | 0.97  | 3794. | 0.51   | 3.69   | 2.11   | 3.18   | 1.60   | 0.7    | 1.58   | 1.99   | 2.90   | 2.39   | 0.79   | 0.32  |
| 67.1  | 1.15  | 3798. | 0.57   | 3.88   | 2.11   | 3.31   | 1.54   | 0.8    | 1.77   | 2.15   | 2.99   | 2.43   | 0.88   | 0.32  |
| 71.5  | 1.25  | 3801. | 0.61   | 3.99   | 2.11   | 3.39   | 1.50   | 0.9    | 1.88   | 2.25   | 3.05   | 2.44   | 0.94   | 0.32  |
| 77.3  | 1.45  | 3806. | 0.64   | 4.14   | 2.11   | 3.50   | 1.47   | 1.0    | 2.03   | 2.39   | 3.13   | 2.48   | 1.02   | 0.32  |
| 83.1  | 1.73  | 3814. | 0.68   | 4.29   | 2.11   | 3.61   | 1.43   | 1.2    | 2.18   | 2.52   | 3.20   | 2.52   | 1.09   | 0.31  |
| 89.0  | 1.89  | 3818. | 0.70   | 4.44   | 2.11   | 3.74   | 1.41   | 1.3    | 2.33   | 2.65   | 3.28   | 2.58   | 1.17   | 0.30  |
| 93.3  | 2.12  | 3824. | 0.72   | 4.55   | 2.11   | 3.83   | 1.39   | 1.5    | 2.44   | 2.75   | 3.33   | 2.61   | 1.22   | 0.29  |
| 102.1 | 2.48  | 3834. | 0.70   | 4.77   | 2.11   | 4.07   | 1.41   | 1.7    | 2.66   | 2.89   | 3.44   | 2.74   | 1.33   | 0.26  |
| 110.8 | 2.84  | 3844. | 0.72   | 4.99   | 2.11   | 4.27   | 1.39   | 2.0    | 2.88   | 3.07   | 3.55   | 2.83   | 1.44   | 0.25  |
| 118.1 | 3.24  | 3855. | 0.66   | 5.17   | 2.11   | 4.51   | 1.45   | 2.2    | 3.06   | 3.12   | 3.64   | 2.98   | 1.53   | 0.22  |
| 119.4 | 3.93  | 3873. | 0.47   | 5.19   | 2.11   | 4.72   | 1.64   | 2.7    | 3.08   | 2.88   | 3.65   | 3.18   | 1.54   | 0.15  |
| 120.9 | 4.31  | 3884. | 0.40   | 5.22   | 2.11   | 4.82   | 1.71   | 3.0    | 3.11   | 2.82   | 3.67   | 3.27   | 1.56   | 0.13  |
| 123.0 | 4.94  | 3901. | 0.27   | 5.26   | 2.11   | 5.00   | 1.84   | 3.4    | 3.15   | 2.71   | 3.69   | 3.42   | 1.58   | 0.08  |
| 124.5 | 5.32  | 3912. | 0.19   | 5.29   | 2.11   | 5.10   | 1.92   | 3.7    | 3.18   | 2.66   | 3.70   | 3.51   | 1.59   | 0.06  |
| 125.6 | 5.68  | 3922. | 0.08   | 5.31   | 2.11   | 5.24   | 2.03   | 3.9    | 3.20   | 2.57   | 3.71   | 3.64   | 1.60   | 0.02  |
| 127.0 | 5.94  | 3930. | 0.02   | 5.34   | 2.11   | 5.32   | 2.09   | 4.1    | 3.23   | 2.55   | 3.73   | 3.71   | 1.62   | 0.01  |
| 127.9 | 6.41  | 3943. | -0.04  | 5.35   | 2.11   | 5.39   | 2.15   | 4.4    | 3.24   | 2.51   | 3.73   | 3.77   | 1.62   | -0.01 |
| 128.7 | 6.91  | 3957. | -0.21  | 5.36   | 2.11   | 5.57   | 2.32   | 4.8    | 3.25   | 2.40   | 3.74   | 3.94   | 1.63   | -0.06 |
| 131.3 | 7.55  | 3976. | -0.34  | 5.41   | 2.11   | 5.75   | 2.45   | 5.2    | 3.30   | 2.35   | 3.76   | 4.10   | 1.65   | -0.10 |
| 133.4 | 8.12  | 3992. | -0.51  | 5.45   | 2.11   | 5.96   | 2.62   | 5.6    | 3.34   | 2.27   | 3.78   | 4.29   | 1.67   | -0.15 |
| 135.7 | 8.74  | 4011. | -0.66  | 5.49   | 2.11   | 6.16   | 2.77   | 6.0    | 3.38   | 2.22   | 3.80   | 4.46   | 1.69   | -0.20 |
| 138.3 | 9.43  | 4031. | -0.79  | 5.54   | 2.11   | 6.33   | 2.90   | 6.5    | 3.43   | 2.18   | 3.83   | 4.62   | 1.72   | -0.23 |
| 139.8 | 10.05 | 4050. | -0.93  | 5.56   | 2.11   | 6.49   | 3.04   | 7.0    | 3.45   | 2.14   | 3.84   | 4.76   | 1.73   | -0.27 |
| 141.7 | 10.67 | 4068. | -1.10  | 5.59   | 2.11   | 6.69   | 3.21   | 7.4    | 3.48   | 2.09   | 3.85   | 4.95   | 1.74   | -0.31 |
| 142.3 | 11.26 | 4086. | -1.23  | 5.59   | 2.11   | 6.82   | 3.34   | 7.8    | 3.48   | 2.04   | 3.85   | 5.08   | 1.74   | -0.35 |
| 143.3 | 12.19 | 4115. | -1.50  | 5.59   | 2.11   | 7.09   | 3.61   | 8.4    | 3.48   | 1.96   | 3.85   | 5.35   | 1.74   | -0.43 |
| 140.7 | 13.79 | 4165. | -1.51  | 5.49   | 2.11   | 7.00   | 3.62   | 9.5    | 3.38   | 1.93   | 3.80   | 5.31   | 1.69   | -0.45 |
| 137.6 | 13.42 | 4154. | -1.63  | 5.42   | 2.11   | 7.05   | 3.74   | 9.3    | 3.31   | 1.89   | 3.77   | 5.39   | 1.66   | -0.49 |
| 135.7 | 14.04 | 4173. | -1.70  | 5.36   | 2.11   | 7.06   | 3.81   | 9.7    | 3.25   | 1.85   | 3.74   | 5.44   | 1.63   | -0.52 |
| 133.5 | 14.70 | 4195. | -1.76  | 5.29   | 2.11   | 7.05   | 3.87   | 10.2   | 3.18   | 1.82   | 3.70   | 5.46   | 1.59   | -0.55 |
| 132.9 | 15.33 | 4215. | -1.83  | 5.26   | 2.11   | 7.10   | 3.94   | 10.6   | 3.15   | 1.80   | 3.69   | 5.52   | 1.58   | -0.58 |
| 129.0 | 15.63 | 4225. | -1.85  | 5.16   | 2.11   | 7.02   | 3.96   | 10.8   | 3.05   | 1.77   | 3.64   | 5.49   | 1.53   | -0.61 |

PROJECT: KENNICOTT GEOTECHNICAL  
 BORING: S-1  
 SAMPLE: S-1  
 DEPTH: 23-25  
 SOIL DESC: CLAYEY SILT TRACE FINE SAND -  
 LT. YELLOW BROWN & WHITE (ML)

STS JOB NO: 25331  
 DATE: 3-1-88  
 TESTED BY: JJ  
 APPROVED BY: JJ

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS | INITIAL | CONSOLIDATED |         |
|--------------------------|---------|--------------|---------|
| DIAMETER-AVERAGE         | MM      | 71.440       | 69.683  |
| LENGTH---AVERAGE         | MM      | 140.000      | 138.320 |
| AREA                     | CM2     | 40.084       | 38.137  |
| VOLUME                   | CM3     | 561.178      | 527.508 |
| WET DENSITY              | G/CM3   | 2.160        | 2.296   |
| DRY DENSITY              | G/CM3   | 1.913        | 2.035   |
| WATER CONTENT            | %       | 12.900       | 12.800  |

| TEST PARAMETERS FOR CONSOLIDATION |        |       |
|-----------------------------------|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 | 7.510 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 | 7.510 |
| BACK PRESSURE                     | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 | 3.510 |
| EFFECTIVE SIGMA 3                 | KG/CM2 | 3.510 |
| CONSOLIDATION RATIO               |        | 1.000 |
| STRAIN RATE                       | MM/MIN | 0.100 |

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BORING:  
 SAMPLE: S-1  
 DEPTH: 23-25

STS JOB NO: 25331  
 EFF. SIGMA3: 3.510 KG/CM2



STS Consultants Ltd.

TEST RESULTS

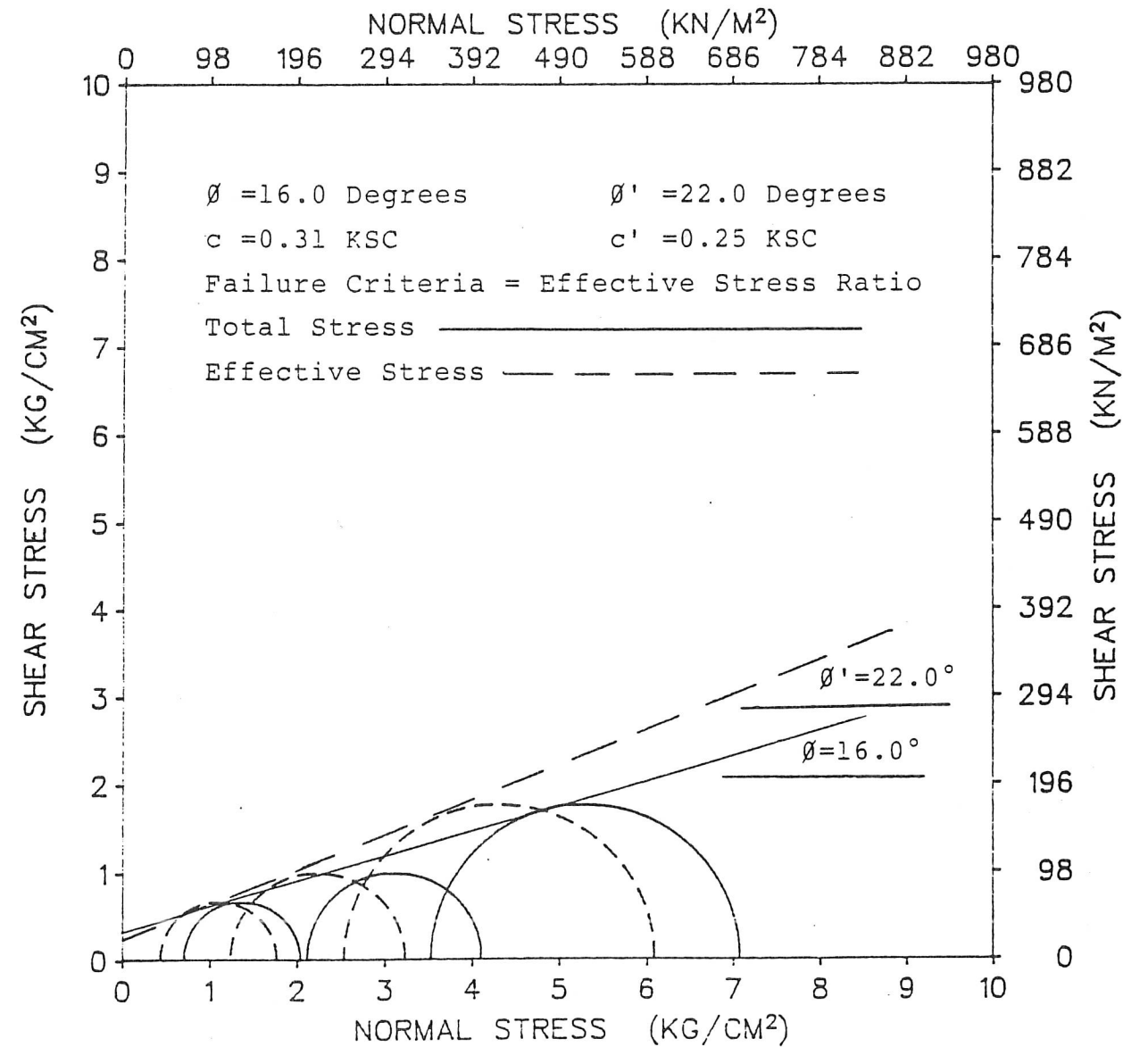
| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P      | PBAR   | Q OR   | A      |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| KG    | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | KG/CM2 | S3     | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |
| 0.0   | 0.00  | 3814. | 0.00   | 3.51   | 3.51   | 3.51   | 3.51   | 0.0    | 0.00   | 1.00   | 3.51   | 3.51   | 0.00   | 0.00   |
| 11.9  | 0.11  | 3817. | 0.39   | 3.82   | 3.51   | 3.43   | 3.12   | 0.1    | 0.31   | 1.10   | 3.67   | 3.27   | 0.16   | 1.25   |
| 25.3  | 0.20  | 3819. | 0.46   | 4.17   | 3.51   | 3.71   | 3.05   | 0.1    | 0.66   | 1.22   | 3.84   | 3.38   | 0.33   | 0.70   |
| 37.2  | 0.29  | 3822. | 0.60   | 4.48   | 3.51   | 3.88   | 2.91   | 0.2    | 0.97   | 1.33   | 4.00   | 3.39   | 0.49   | 0.62   |
| 49.1  | 0.42  | 3825. | 0.75   | 4.79   | 3.51   | 4.05   | 2.76   | 0.3    | 1.28   | 1.46   | 4.15   | 3.41   | 0.64   | 0.58   |
| 59.5  | 0.52  | 3828. | 0.91   | 5.06   | 3.51   | 4.16   | 2.60   | 0.4    | 1.55   | 1.60   | 4.29   | 3.38   | 0.78   | 0.58   |
| 65.4  | 0.62  | 3831. | 0.96   | 5.22   | 3.51   | 4.26   | 2.55   | 0.4    | 1.71   | 1.67   | 4.36   | 3.40   | 0.85   | 0.56   |
| 74.4  | 0.77  | 3835. | 1.07   | 5.45   | 3.51   | 4.38   | 2.44   | 0.6    | 1.94   | 1.79   | 4.48   | 3.41   | 0.97   | 0.55   |
| 89.2  | 1.08  | 3844. | 1.16   | 5.83   | 3.51   | 4.68   | 2.36   | 0.8    | 2.32   | 1.99   | 4.67   | 3.52   | 1.16   | 0.50   |
| 96.7  | 1.28  | 3849. | 1.19   | 6.02   | 3.51   | 4.83   | 2.32   | 0.9    | 2.51   | 2.08   | 4.77   | 3.58   | 1.26   | 0.47   |
| 104.1 | 1.49  | 3855. | 1.21   | 6.21   | 3.51   | 5.00   | 2.30   | 1.1    | 2.70   | 2.17   | 4.86   | 3.65   | 1.35   | 0.45   |
| 110.1 | 1.66  | 3860. | 1.21   | 6.36   | 3.51   | 5.15   | 2.30   | 1.2    | 2.85   | 2.24   | 4.94   | 3.73   | 1.43   | 0.42   |
| 117.5 | 1.94  | 3868. | 1.21   | 6.55   | 3.51   | 5.34   | 2.30   | 1.4    | 3.04   | 2.32   | 5.03   | 3.82   | 1.52   | 0.40   |
| 126.4 | 2.19  | 3875. | 1.19   | 6.77   | 3.51   | 5.58   | 2.32   | 1.6    | 3.26   | 2.41   | 5.14   | 3.95   | 1.63   | 0.36   |
| 136.9 | 2.58  | 3886. | 1.17   | 7.03   | 3.51   | 5.86   | 2.34   | 1.9    | 3.52   | 2.51   | 5.27   | 4.10   | 1.76   | 0.33   |
| 145.8 | 2.96  | 3897. | 1.14   | 7.25   | 3.51   | 6.11   | 2.37   | 2.1    | 3.74   | 2.58   | 5.38   | 4.24   | 1.87   | 0.30   |
| 153.2 | 3.37  | 3909. | 1.08   | 7.43   | 3.51   | 6.35   | 2.43   | 2.4    | 3.92   | 2.62   | 5.47   | 4.39   | 1.96   | 0.28   |
| 160.7 | 3.80  | 3921. | 1.07   | 7.61   | 3.51   | 6.54   | 2.44   | 2.7    | 4.10   | 2.68   | 5.56   | 4.49   | 2.05   | 0.26   |
| 165.1 | 4.18  | 3932. | 1.03   | 7.71   | 3.51   | 6.68   | 2.48   | 3.0    | 4.20   | 2.69   | 5.61   | 4.58   | 2.10   | 0.25   |
| 169.6 | 4.63  | 3946. | 1.00   | 7.81   | 3.51   | 6.81   | 2.51   | 3.3    | 4.30   | 2.71   | 5.66   | 4.66   | 2.15   | 0.23   |
| 174.1 | 5.00  | 3957. | 0.96   | 7.91   | 3.51   | 6.95   | 2.55   | 3.6    | 4.40   | 2.72   | 5.71   | 4.75   | 2.20   | 0.22   |
| 178.5 | 5.44  | 3970. | 0.92   | 8.01   | 3.51   | 7.08   | 2.59   | 3.9    | 4.50   | 2.74   | 5.76   | 4.83   | 2.25   | 0.21   |
| 181.5 | 5.81  | 3981. | 0.89   | 8.07   | 3.51   | 7.18   | 2.62   | 4.2    | 4.56   | 2.74   | 5.79   | 4.90   | 2.28   | 0.19   |
| 184.5 | 6.28  | 3995. | 0.84   | 8.13   | 3.51   | 7.29   | 2.68   | 4.5    | 4.62   | 2.73   | 5.82   | 4.98   | 2.31   | 0.18   |
| 187.5 | 6.86  | 4013. | 0.78   | 8.18   | 3.51   | 7.40   | 2.73   | 5.0    | 4.67   | 2.71   | 5.85   | 5.06   | 2.34   | 0.17   |
| 191.9 | 7.52  | 4033. | 0.73   | 8.27   | 3.51   | 7.54   | 2.78   | 5.4    | 4.76   | 2.71   | 5.89   | 5.16   | 2.38   | 0.15   |
| 193.4 | 8.12  | 4052. | 0.68   | 8.28   | 3.51   | 7.61   | 2.84   | 5.9    | 4.77   | 2.68   | 5.90   | 5.22   | 2.39   | 0.14   |
| 194.9 | 8.76  | 4072. | 0.62   | 8.30   | 3.51   | 7.67   | 2.89   | 6.3    | 4.79   | 2.66   | 5.90   | 5.28   | 2.39   | 0.13   |
| 196.4 | 9.30  | 4089. | 0.57   | 8.31   | 3.51   | 7.75   | 2.94   | 6.7    | 4.80   | 2.63   | 5.91   | 5.34   | 2.40   | 0.12   |
| 199.3 | 10.20 | 4117. | 0.52   | 8.35   | 3.51   | 7.84   | 2.99   | 7.4    | 4.84   | 2.62   | 5.93   | 5.42   | 2.42   | 0.11   |
| 199.3 | 11.20 | 4150. | 0.46   | 8.31   | 3.51   | 7.85   | 3.05   | 8.1    | 4.80   | 2.58   | 5.91   | 5.45   | 2.40   | 0.10   |
| 200.8 | 11.84 | 4171. | 0.41   | 8.32   | 3.51   | 7.92   | 3.10   | 8.6    | 4.81   | 2.55   | 5.92   | 5.51   | 2.41   | 0.08   |
| 202.3 | 12.48 | 4192. | 0.39   | 8.34   | 3.51   | 7.94   | 3.12   | 9.0    | 4.83   | 2.55   | 5.92   | 5.53   | 2.41   | 0.08   |
| 202.3 | 13.00 | 4209. | 0.34   | 8.32   | 3.51   | 7.98   | 3.17   | 9.4    | 4.81   | 2.51   | 5.91   | 5.58   | 2.40   | 0.07   |
| 203.8 | 13.70 | 4233. | 0.32   | 8.32   | 3.51   | 8.00   | 3.19   | 9.9    | 4.81   | 2.51   | 5.92   | 5.60   | 2.41   | 0.07   |
| 206.8 | 14.28 | 4253. | 0.30   | 8.37   | 3.51   | 8.07   | 3.21   | 10.3   | 4.86   | 2.52   | 5.94   | 5.64   | 2.43   | 0.06   |
| 206.8 | 14.90 | 4274. | 0.27   | 8.35   | 3.51   | 8.08   | 3.24   | 10.8   | 4.84   | 2.49   | 5.93   | 5.66   | 2.42   | 0.05   |
| 205.3 | 15.54 | 4296. | 0.25   | 8.29   | 3.51   | 8.04   | 3.26   | 11.2   | 4.78   | 2.47   | 5.90   | 5.65   | 2.39   | 0.05   |
| 203.8 | 16.49 | 4330. | 0.21   | 8.22   | 3.51   | 8.00   | 3.30   | 11.9   | 4.71   | 2.43   | 5.86   | 5.65   | 2.35   | 0.05   |
| 202.3 | 17.40 | 4362. | 0.18   | 8.15   | 3.51   | 7.97   | 3.33   | 12.6   | 4.64   | 2.39   | 5.83   | 5.65   | 2.32   | 0.04   |
| 200.8 | 18.30 | 4395. | 0.14   | 8.08   | 3.51   | 7.94   | 3.37   | 13.2   | 4.57   | 2.36   | 5.79   | 5.65   | 2.28   | 0.03   |
| 197.9 | 19.00 | 4421. | 0.14   | 7.99   | 3.51   | 7.84   | 3.37   | 13.7   | 4.48   | 2.33   | 5.75   | 5.61   | 2.24   | 0.03   |
| 197.9 | 20.58 | 4480. | 0.12   | 7.93   | 3.51   | 7.80   | 3.39   | 14.9   | 4.42   | 2.30   | 5.72   | 5.59   | 2.21   | 0.03   |
| 196.4 | 21.20 | 4504. | 0.11   | 7.87   | 3.51   | 7.76   | 3.40   | 15.3   | 4.36   | 2.28   | 5.69   | 5.58   | 2.18   | 0.02   |

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

Boring: S-3                      Sample: 3                      Depth: 36-37  
 Boring: S3                        Sample: S3                      Depth: 37-38  
 Boring:                            Sample: 3                        Depth: 38-39

MOHR ENVELOPE



Sigma 3 = 0.7 ksc  
 Sigma 3 = 2.1 ksc  
 Sigma 3 = 3.5 ksc



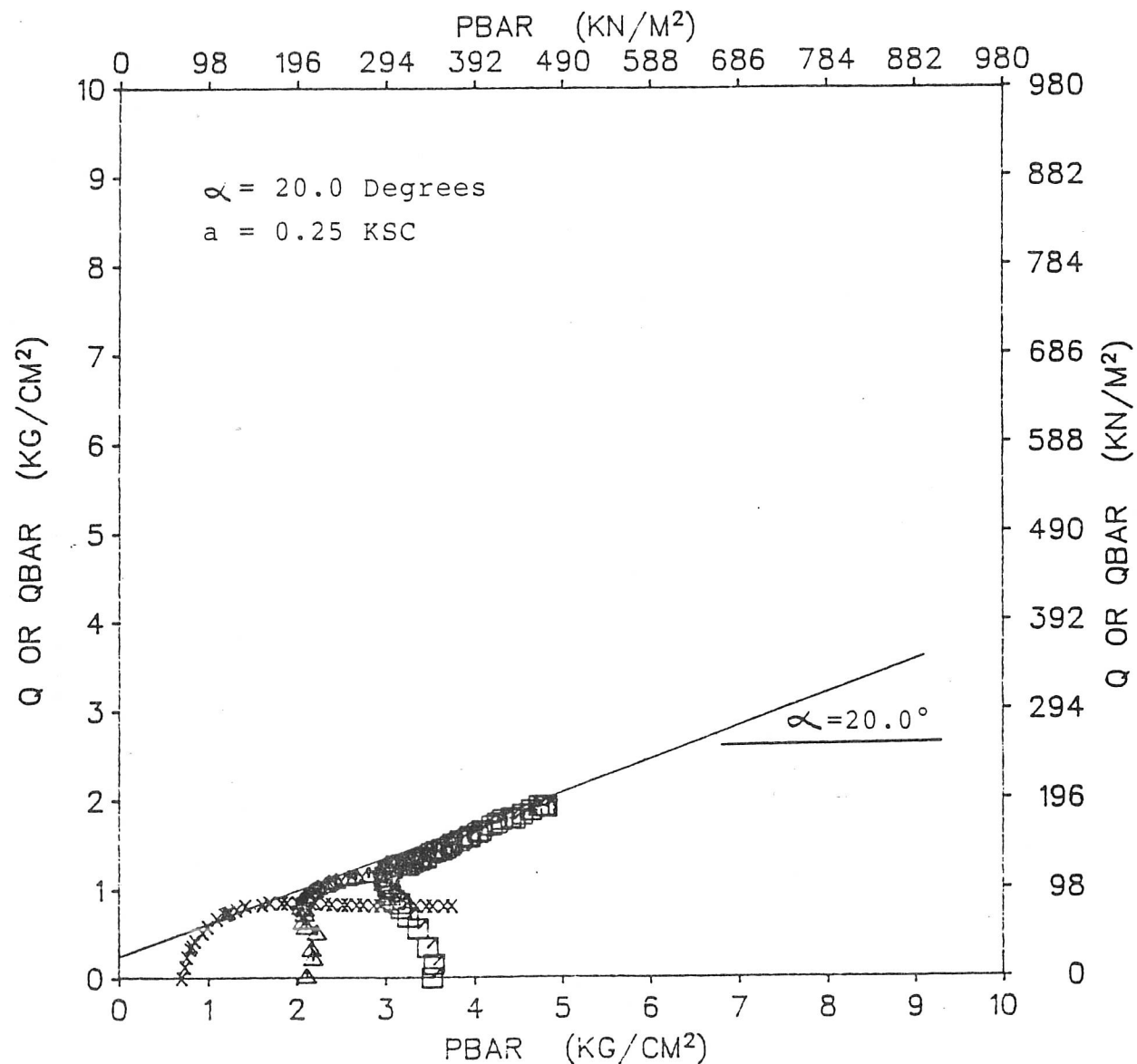
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |            |              |
|-------------|------------|--------------|
| Boring: S-3 | Sample: 3  | Depth: 36-37 |
| Boring: S3  | Sample: S3 | Depth: 37-38 |
| Boring:     | Sample: 3  | Depth: 38-39 |

STRESS PATH PLOT



x Sigma 3 = 0.7 ksc  
 $\Delta$  Sigma 3 = 2.1 ksc  
 $\square$  Sigma 3 = 3.5 ksc



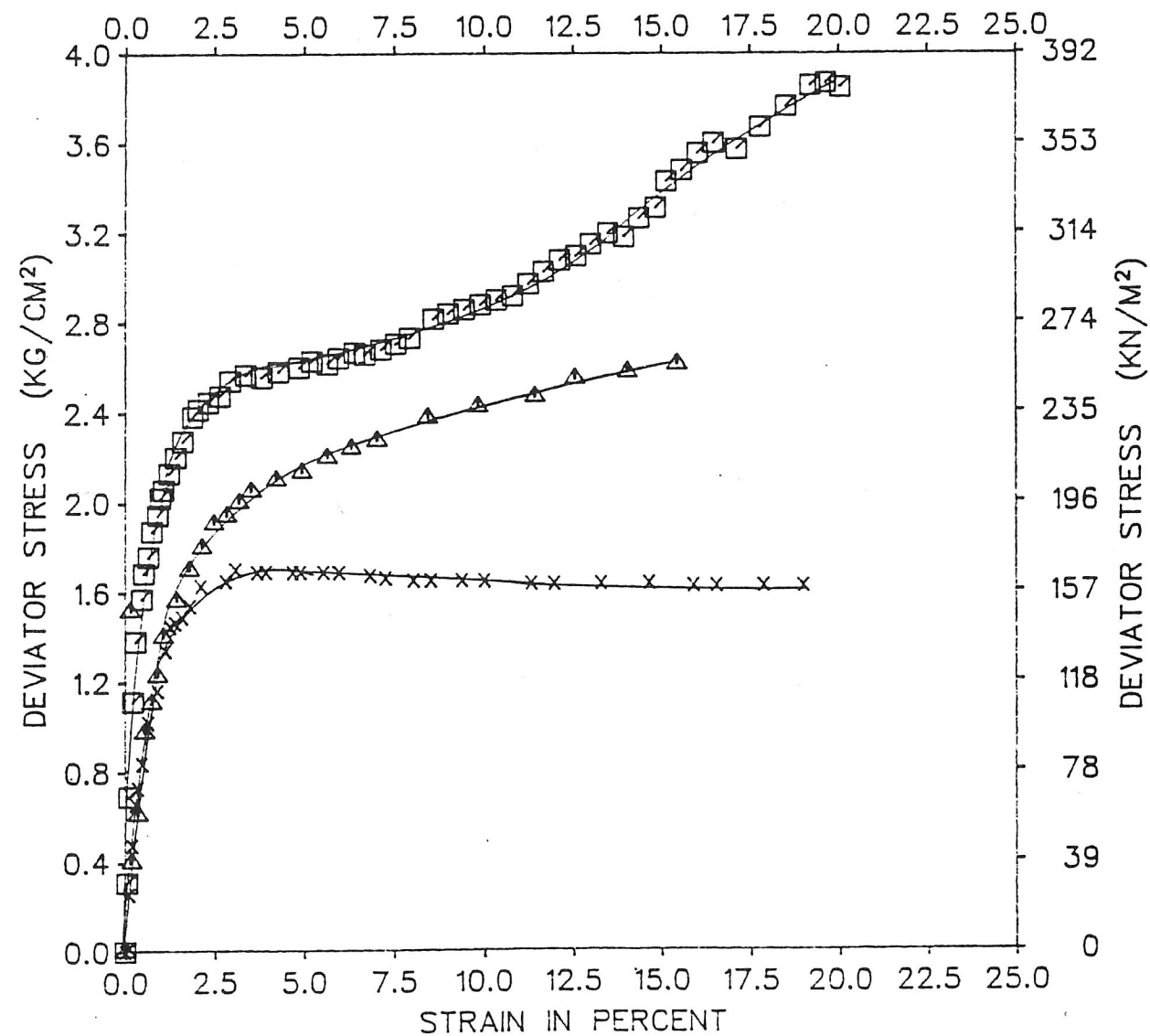
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |            |              |
|-------------|------------|--------------|
| Boring: S-3 | Sample: 3  | Depth: 36-37 |
| Boring: S3  | Sample: S3 | Depth: 37-38 |
| Boring:     | Sample: 3  | Depth: 38-39 |

DEVIATOR STRESS vs STRAIN



x Sigma 3 = 0.7 ksc  
 $\Delta$  Sigma 3 = 2.1 ksc  
 $\square$  Sigma 3 = 3.5 ksc



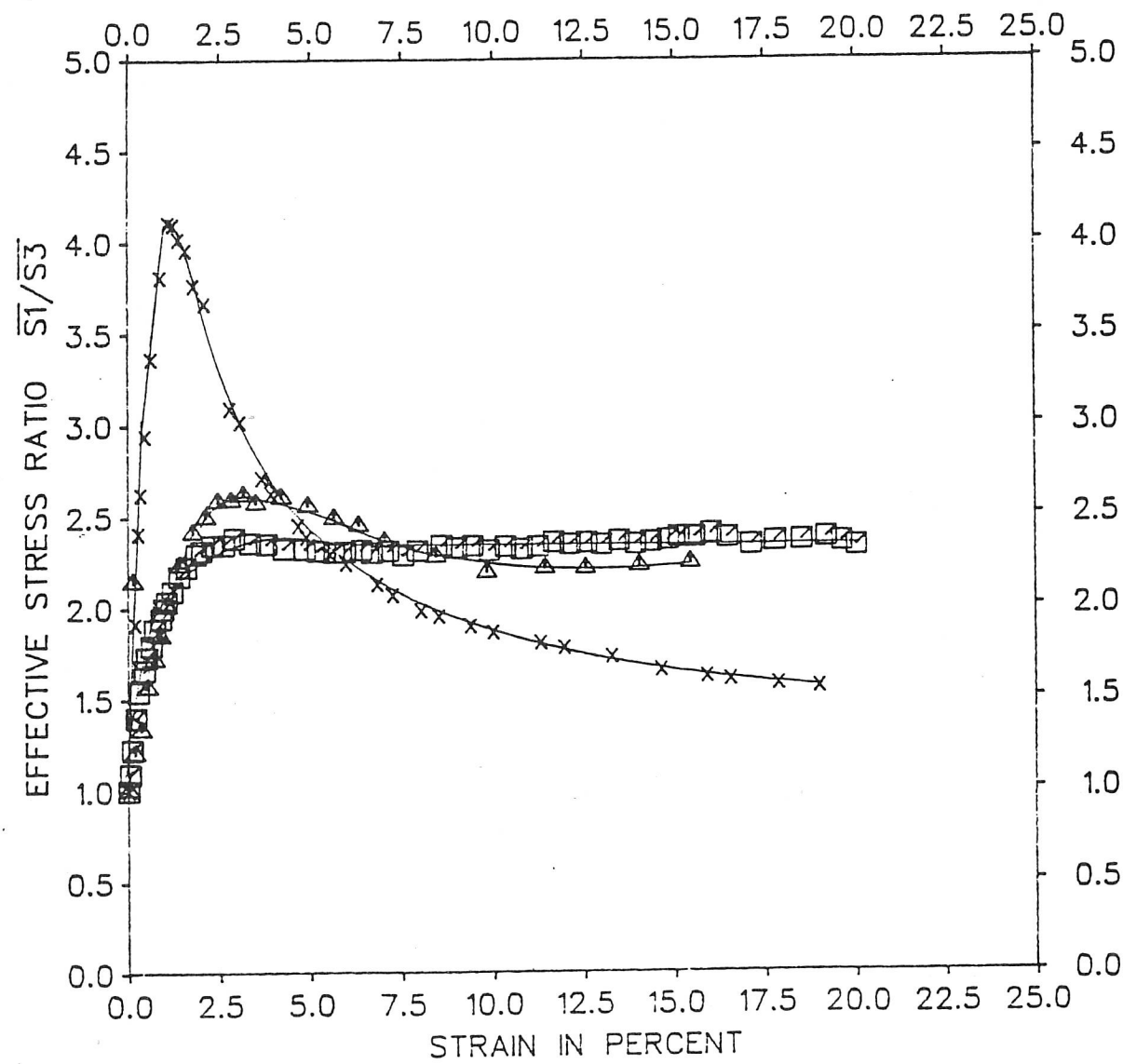
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |            |              |
|-------------|------------|--------------|
| Boring: S-3 | Sample: 3  | Depth: 36-37 |
| Boring: S3  | Sample: S3 | Depth: 37-38 |
| Boring:     | Sample: 3  | Depth: 38-39 |

EFFECTIVE STRESS RATIO vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.1 ksc  
 ◻ Sigma 3 = 3.5 ksc

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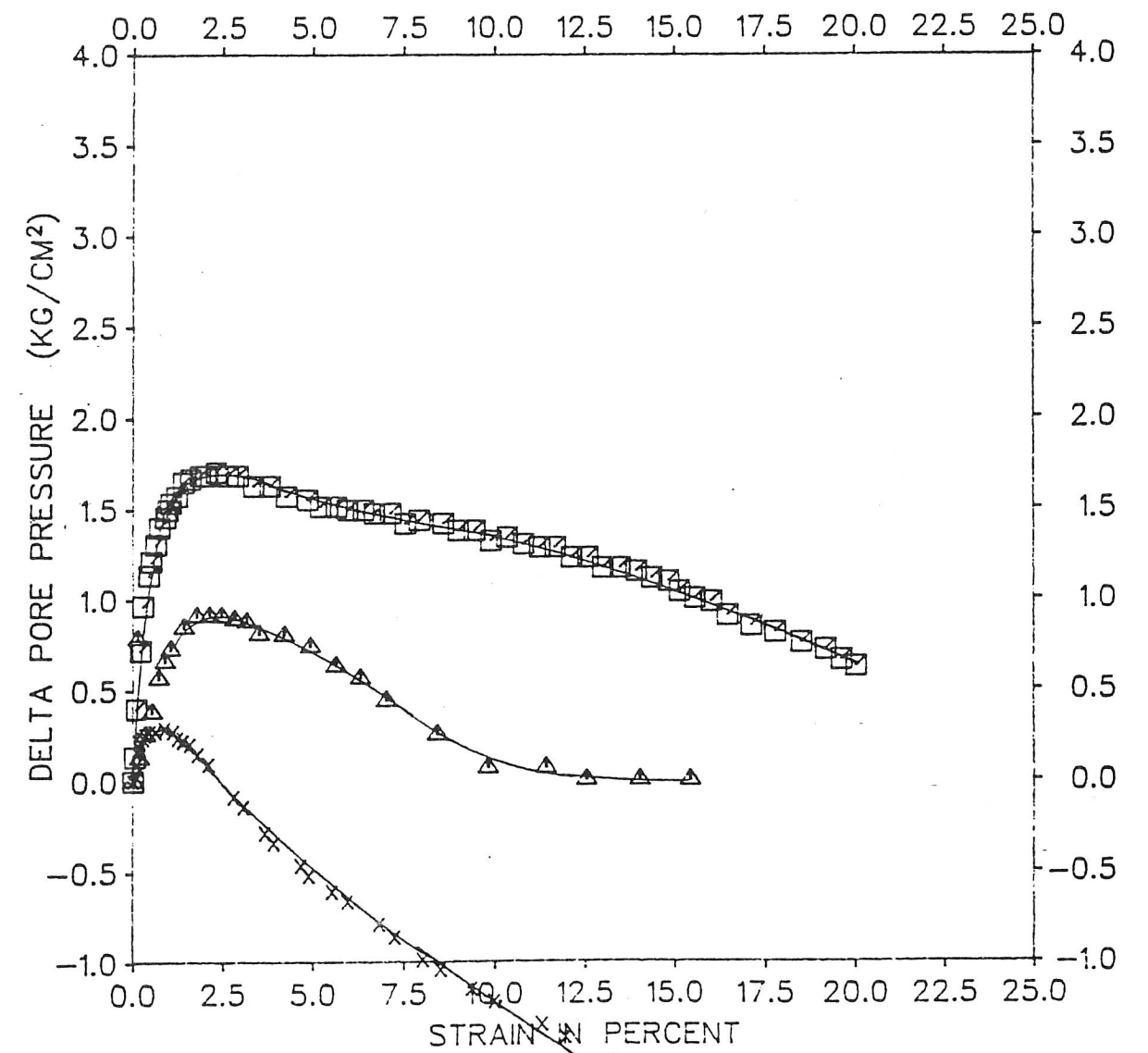
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |            |              |
|-------------|------------|--------------|
| Boring: S-3 | Sample: 3  | Depth: 36-37 |
| Boring: S3  | Sample: S3 | Depth: 37-38 |
| Boring:     | Sample: 3  | Depth: 38-39 |

DELTA PORE PRESSURE vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.1 ksc  
 ◻ Sigma 3 = 3.5 ksc

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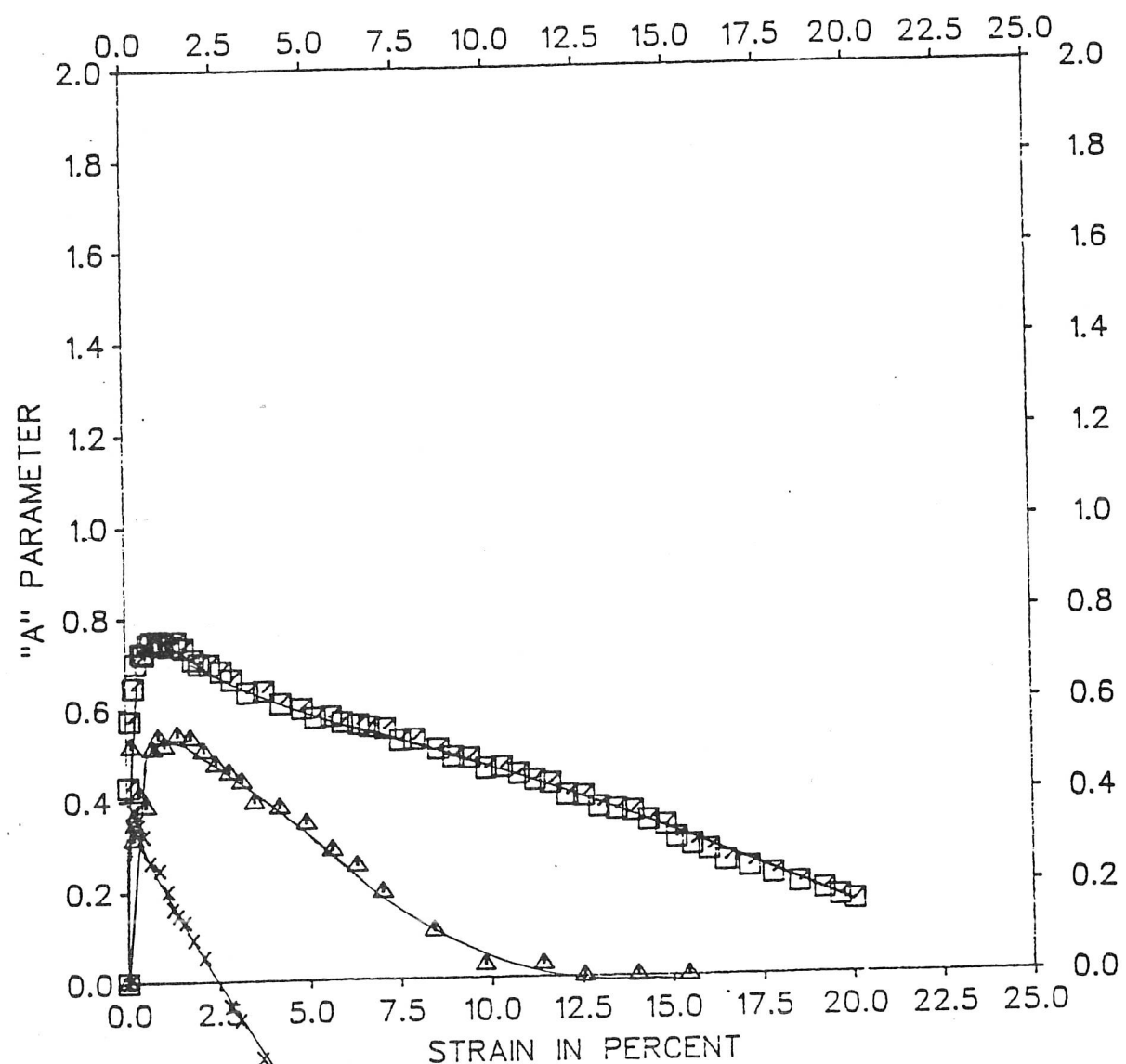
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STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

Boring: S-3            Sample: 3            Depth: 36-37  
 Boring: S3            Sample: S3            Depth: 37-38  
 Boring:                Sample: 3            Depth: 38-39

"A" PARAMETER vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.7 ksc  
 □ Sigma 3 = 3.5 ksc

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TRIAXIAL COMPRESSION TEST  
CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
 BORING: S-3  
 SAMPLE: 3  
 DEPTH: 36-37  
 SOIL DESC: SILT TRACE CLAY TRACE FINE SAND &  
 FINE GRAVEL - BROWN (ML)

STS JOB NO: 25331  
 DATE: 3-7-88  
 TESTED BY: JJ  
 APPROVED BY: *[Signature]*

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS |       | INITIAL | CONSOLIDATED |
|--------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE         | MM    | 73.250  | 73.046       |
| LENGTH---AVERAGE         | MM    | 144.000 | 143.900      |
| AREA                     | CM2   | 42.141  | 41.907       |
| VOLUME                   | CM3   | 606.831 | 603.039      |
| WET DENSITY              | G/CM3 | 2.193   | 2.247        |
| DRY DENSITY              | G/CM3 | 1.935   | 1.947        |
| WATER CONTENT            | %     | 13.300  | 15.400       |

| TEST PARAMETERS FOR CONSOLIDATION |        |       |
|-----------------------------------|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 | 4.700 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 | 4.700 |
| BACK PRESSURE                     | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 | 0.700 |
| EFFECTIVE SIGMA 3                 | KG/CM2 | 0.700 |
| CONSOLIDATION RATIO               |        | 1.000 |
| STRAIN RATE                       | MM/MIN | 0.100 |

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BORING: 3-3  
 SAMPLE: 3  
 DEPTH: 36-37

STS JOB NO: 25331  
 EFF. SIGMA3: 0.700 KG/CM2

STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
 CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
 BORING: S3  
 SAMPLE: S3  
 DEPTH: 37-38

STS JOB NO: 25331  
 DATE: 3-7-88  
 TESTED BY: JJ  
 APPROVED BY: AS

SOIL DESC: SILT TRACE CLAY TRACE F-M SAND  
 & FINE GRAVEL - BROWN (ML)

TEST RESULTS-----

| LOAD | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 - | S1BAR/ | P      | PBAR   | Q OR   | A     |
|------|-------|-------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|-------|
| KG   | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | S3   | S3BAR  | KG/CM2 | KG/CM2 | KG/CM2 |       |
| 0.0  | 0.00  | 4191. | 0.00   | 0.70   | 0.70   | 0.70   | 0.70   | 0.0    | 0.00 | 1.00   | 0.70   | 0.70   | 0.00   | 0.00  |
| 10.7 | 0.14  | 4195. | 0.09   | 0.96   | 0.70   | 0.87   | 0.61   | 0.1    | 0.26 | 1.42   | 0.83   | 0.74   | 0.13   | 0.35  |
| 19.9 | 0.26  | 4198. | 0.18   | 1.17   | 0.70   | 1.00   | 0.52   | 0.2    | 0.47 | 1.91   | 0.94   | 0.76   | 0.24   | 0.38  |
| 27.6 | 0.40  | 4202. | 0.23   | 1.36   | 0.70   | 1.12   | 0.47   | 0.3    | 0.66 | 2.41   | 1.03   | 0.80   | 0.33   | 0.35  |
| 30.6 | 0.48  | 4205. | 0.25   | 1.43   | 0.70   | 1.18   | 0.45   | 0.3    | 0.73 | 2.62   | 1.06   | 0.81   | 0.36   | 0.34  |
| 35.2 | 0.66  | 4210. | 0.27   | 1.54   | 0.70   | 1.27   | 0.43   | 0.5    | 0.84 | 2.94   | 1.12   | 0.85   | 0.42   | 0.32  |
| 42.9 | 0.90  | 4217. | 0.27   | 1.72   | 0.70   | 1.45   | 0.43   | 0.6    | 1.02 | 3.36   | 1.21   | 0.94   | 0.51   | 0.26  |
| 49.0 | 1.27  | 4228. | 0.29   | 1.86   | 0.70   | 1.57   | 0.41   | 0.9    | 1.16 | 3.81   | 1.28   | 0.99   | 0.58   | 0.25  |
| 56.7 | 1.59  | 4238. | 0.27   | 2.04   | 0.70   | 1.77   | 0.43   | 1.1    | 1.34 | 4.10   | 1.37   | 1.10   | 0.67   | 0.20  |
| 61.3 | 1.77  | 4243. | 0.23   | 2.14   | 0.70   | 1.91   | 0.47   | 1.2    | 1.44 | 4.09   | 1.42   | 1.19   | 0.72   | 0.16  |
| 62.1 | 1.97  | 4249. | 0.22   | 2.16   | 0.70   | 1.95   | 0.48   | 1.4    | 1.46 | 4.01   | 1.43   | 1.22   | 0.73   | 0.15  |
| 63.3 | 2.25  | 4257. | 0.20   | 2.19   | 0.70   | 1.99   | 0.50   | 1.6    | 1.49 | 3.96   | 1.44   | 1.25   | 0.74   | 0.13  |
| 65.6 | 2.57  | 4267. | 0.14   | 2.24   | 0.70   | 2.09   | 0.56   | 1.8    | 1.54 | 3.76   | 1.47   | 1.33   | 0.77   | 0.09  |
| 69.6 | 3.01  | 4280. | 0.09   | 2.33   | 0.70   | 2.24   | 0.61   | 2.1    | 1.63 | 3.66   | 1.51   | 1.42   | 0.81   | 0.05  |
| 71.1 | 4.02  | 4311. | -0.09  | 2.35   | 0.70   | 2.44   | 0.79   | 2.8    | 1.65 | 3.09   | 1.52   | 1.61   | 0.82   | -0.05 |
| 73.5 | 4.42  | 4323. | -0.14  | 2.40   | 0.70   | 2.54   | 0.84   | 3.1    | 1.70 | 3.01   | 1.55   | 1.69   | 0.85   | -0.08 |
| 73.4 | 5.28  | 4350. | -0.29  | 2.39   | 0.70   | 2.68   | 0.99   | 3.7    | 1.69 | 2.71   | 1.54   | 1.83   | 0.84   | -0.17 |
| 73.7 | 5.64  | 4362. | -0.34  | 2.39   | 0.70   | 2.73   | 1.04   | 3.9    | 1.69 | 2.62   | 1.54   | 1.89   | 0.84   | -0.20 |
| 74.2 | 6.71  | 4396. | -0.47  | 2.39   | 0.70   | 2.86   | 1.17   | 4.7    | 1.69 | 2.45   | 1.54   | 2.01   | 0.84   | -0.28 |
| 74.4 | 7.03  | 4406. | -0.52  | 2.39   | 0.70   | 2.91   | 1.22   | 4.9    | 1.69 | 2.38   | 1.54   | 2.07   | 0.84   | -0.31 |
| 74.9 | 7.95  | 4436. | -0.61  | 2.39   | 0.70   | 3.00   | 1.31   | 5.5    | 1.69 | 2.29   | 1.54   | 2.16   | 0.84   | -0.36 |
| 75.2 | 8.58  | 4456. | -0.66  | 2.39   | 0.70   | 3.05   | 1.36   | 6.0    | 1.69 | 2.24   | 1.54   | 2.21   | 0.84   | -0.39 |
| 75.3 | 9.82  | 4498. | -0.79  | 2.37   | 0.70   | 3.16   | 1.49   | 6.8    | 1.67 | 2.12   | 1.54   | 2.33   | 0.84   | -0.47 |
| 75.1 | 10.44 | 4518. | -0.86  | 2.36   | 0.70   | 3.22   | 1.56   | 7.3    | 1.66 | 2.06   | 1.53   | 2.39   | 0.83   | -0.52 |
| 75.2 | 11.55 | 4556. | -0.99  | 2.35   | 0.70   | 3.34   | 1.69   | 8.0    | 1.65 | 1.98   | 1.53   | 2.51   | 0.83   | -0.60 |
| 75.6 | 12.24 | 4580. | -1.04  | 2.35   | 0.70   | 3.39   | 1.74   | 8.5    | 1.65 | 1.95   | 1.53   | 2.57   | 0.83   | -0.63 |
| 76.3 | 13.48 | 4624. | -1.15  | 2.35   | 0.70   | 3.50   | 1.85   | 9.4    | 1.65 | 1.89   | 1.53   | 2.67   | 0.83   | -0.70 |
| 76.8 | 14.38 | 4656. | -1.22  | 2.35   | 0.70   | 3.57   | 1.92   | 10.0   | 1.65 | 1.86   | 1.52   | 2.75   | 0.82   | -0.74 |
| 77.4 | 16.27 | 4725. | -1.35  | 2.34   | 0.70   | 3.69   | 2.05   | 11.3   | 1.64 | 1.80   | 1.52   | 2.87   | 0.82   | -0.82 |
| 77.9 | 17.21 | 4760. | -1.42  | 2.34   | 0.70   | 3.76   | 2.12   | 12.0   | 1.64 | 1.77   | 1.52   | 2.94   | 0.82   | -0.87 |
| 79.1 | 19.10 | 4832. | -1.56  | 2.34   | 0.70   | 3.90   | 2.26   | 13.3   | 1.64 | 1.72   | 1.52   | 3.08   | 0.82   | -0.95 |
| 80.4 | 21.06 | 4909. | -1.81  | 2.34   | 0.70   | 4.15   | 2.51   | 14.6   | 1.64 | 1.65   | 1.52   | 3.33   | 0.82   | -1.11 |
| 81.0 | 22.87 | 4983. | -1.94  | 2.33   | 0.70   | 4.26   | 2.64   | 15.9   | 1.63 | 1.62   | 1.51   | 3.45   | 0.81   | -1.19 |
| 81.6 | 23.80 | 5021. | -2.01  | 2.33   | 0.70   | 4.34   | 2.71   | 16.5   | 1.63 | 1.60   | 1.51   | 3.52   | 0.81   | -1.24 |
| 82.9 | 25.70 | 5102. | -2.14  | 2.32   | 0.70   | 4.46   | 2.84   | 17.9   | 1.62 | 1.57   | 1.51   | 3.65   | 0.81   | -1.32 |
| 84.0 | 27.31 | 5172. | -2.23  | 2.32   | 0.70   | 4.55   | 2.93   | 19.0   | 1.62 | 1.56   | 1.51   | 3.74   | 0.81   | -1.37 |

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS----- |       | INITIAL | CONSOLIDATED |
|-------------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE              | MM    | 72.090  | 71.121       |
| LENGTH---AVERAGE              | MM    | 144.350 | 142.730      |
| AREA                          | CM2   | 40.817  | 39.727       |
| VOLUME                        | CM3   | 589.192 | 567.021      |
| WET DENSITY                   | G/CM3 | 2.147   | 2.206        |
| DRY DENSITY                   | G/CM3 | 1.882   | 1.956        |
| WATER CONTENT                 | %     | 14.100  | 12.800       |

| TEST PARAMETERS FOR CONSOLIDATION----- |        |       |
|--|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE           | KG/CM2 | 6.110 |
| TOTAL SIGMA3 + BACK PRESSURE           | KG/CM2 | 6.110 |
| BACK PRESSURE                          | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                      | KG/CM2 | 2.110 |
| EFFECTIVE SIGMA 3                      | KG/CM2 | 2.110 |
| CONSOLIDATION RATIO                    |        | 1.000 |
| STRAIN RATE                            | MM/MIN | 0.100 |

BORING: S3  
 SAMPLE: S3  
 DEPTH: 37-38

STS JOB NO: 25331  
 EFF. SIGMA3: 2.110 KG/CM2

STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
 CONSOLIDATED UNDRAINED - DATA

TEST RESULTS

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P      | PSAR   | Q OR   | A      |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| KG    | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |
| 0.0   | 0.00  | 3973. | 0.00   | 2.11   | 2.11   | 2.11   | 2.11   | 0.0    | 0.30   | 1.00   | 2.11   | 2.11   | 0.00   | 0.00   |
| 15.9  | 0.25  | 3980. | 0.13   | 2.51   | 2.11   | 2.38   | 1.99   | 0.2    | 0.40   | 1.20   | 2.31   | 2.18   | 0.20   | 0.31   |
| 24.3  | 0.50  | 3987. | 0.25   | 2.72   | 2.11   | 2.47   | 1.86   | 0.4    | 0.61   | 1.33   | 2.41   | 2.16   | 0.30   | 0.41   |
| 38.9  | 0.75  | 3994. | 0.38   | 3.08   | 2.11   | 2.71   | 1.74   | 0.5    | 0.97   | 1.56   | 2.60   | 2.22   | 0.49   | 0.38   |
| 44.2  | 1.02  | 4001. | 0.56   | 3.21   | 2.11   | 2.65   | 1.55   | 0.7    | 1.10   | 1.71   | 2.66   | 2.10   | 0.55   | 0.51   |
| 49.1  | 1.26  | 4008. | 0.66   | 3.34   | 2.11   | 2.68   | 1.45   | 0.9    | 1.23   | 1.84   | 2.72   | 2.07   | 0.61   | 0.54   |
| 56.2  | 1.48  | 4014. | 0.72   | 3.51   | 2.11   | 2.79   | 1.39   | 1.0    | 1.40   | 2.01   | 2.81   | 2.09   | 0.70   | 0.52   |
| 60.3  | 0.18  | 3978. | 0.78   | 3.63   | 2.11   | 2.84   | 1.33   | 0.1    | 1.52   | 2.14   | 2.87   | 2.09   | 0.76   | 0.52   |
| 62.9  | 2.01  | 4029. | 0.84   | 3.67   | 2.11   | 2.83   | 1.27   | 1.4    | 1.56   | 2.23   | 2.89   | 2.05   | 0.78   | 0.54   |
| 68.7  | 2.52  | 4044. | 0.91   | 3.81   | 2.11   | 2.90   | 1.20   | 1.8    | 1.70   | 2.41   | 2.96   | 2.05   | 0.85   | 0.53   |
| 73.0  | 3.03  | 4059. | 0.91   | 3.91   | 2.11   | 3.00   | 1.20   | 2.1    | 1.80   | 2.50   | 3.01   | 2.10   | 0.90   | 0.50   |
| 77.6  | 3.51  | 4073. | 0.91   | 4.02   | 2.11   | 3.11   | 1.20   | 2.5    | 1.91   | 2.58   | 3.06   | 2.16   | 0.95   | 0.48   |
| 79.3  | 4.03  | 4088. | 0.89   | 4.05   | 2.11   | 3.16   | 1.22   | 2.8    | 1.94   | 2.59   | 3.08   | 2.19   | 0.97   | 0.46   |
| 82.0  | 4.52  | 4103. | 0.88   | 4.11   | 2.11   | 3.23   | 1.24   | 3.2    | 2.00   | 2.62   | 3.11   | 2.23   | 1.00   | 0.44   |
| 84.4  | 5.01  | 4117. | 0.81   | 4.16   | 2.11   | 3.35   | 1.30   | 3.5    | 2.05   | 2.57   | 3.13   | 2.33   | 1.02   | 0.39   |
| 87.1  | 6.00  | 4147. | 0.80   | 4.21   | 2.11   | 3.41   | 1.31   | 4.2    | 2.10   | 2.60   | 3.16   | 2.36   | 1.05   | 0.38   |
| 89.2  | 7.03  | 4178. | 0.74   | 4.24   | 2.11   | 3.51   | 1.37   | 4.9    | 2.13   | 2.56   | 3.18   | 2.44   | 1.07   | 0.35   |
| 92.6  | 8.04  | 4210. | 0.63   | 4.31   | 2.11   | 3.68   | 1.48   | 5.6    | 2.20   | 2.49   | 3.21   | 2.58   | 1.10   | 0.29   |
| 95.0  | 9.01  | 4240. | 0.56   | 4.35   | 2.11   | 3.79   | 1.55   | 6.3    | 2.24   | 2.45   | 3.23   | 2.67   | 1.12   | 0.25   |
| 97.2  | 10.02 | 4273. | 0.44   | 4.38   | 2.11   | 3.95   | 1.67   | 7.0    | 2.27   | 2.36   | 3.25   | 2.81   | 1.14   | 0.19   |
| 103.0 | 12.02 | 4338. | 0.25   | 4.48   | 2.11   | 4.23   | 1.86   | 8.4    | 2.37   | 2.28   | 3.30   | 3.05   | 1.19   | 0.11   |
| 106.8 | 14.01 | 4405. | 0.07   | 4.53   | 2.11   | 4.47   | 2.04   | 9.8    | 2.42   | 2.19   | 3.32   | 3.25   | 1.21   | 0.03   |
| 110.7 | 16.30 | 4485. | 0.07   | 4.58   | 2.11   | 4.51   | 2.04   | 11.4   | 2.47   | 2.21   | 3.34   | 3.28   | 1.23   | 0.03   |
| 115.7 | 17.91 | 4543. | 0.00   | 4.66   | 2.11   | 4.66   | 2.11   | 12.5   | 2.55   | 2.21   | 3.38   | 3.38   | 1.27   | 0.00   |
| 119.0 | 20.03 | 4621. | 0.00   | 4.69   | 2.11   | 4.68   | 2.11   | 14.0   | 2.58   | 2.22   | 3.40   | 3.40   | 1.29   | 0.00   |
| 122.6 | 22.03 | 4698. | 0.00   | 4.72   | 2.11   | 4.72   | 2.11   | 15.4   | 2.61   | 2.24   | 3.41   | 3.41   | 1.30   | 0.00   |

PROJECT: KENNICOTT GEOTECHNICAL  
 BORING: 3  
 SAMPLE: 3  
 DEPTH: 38-39  
 SOIL DESC: SILT TRACE CLAY TRACE F-M SAND  
 & FINE GRAVEL - BROWN (ML)

STS JOB NO: 25331  
 DATE: 3-7-88  
 TESTED BY: JJ  
 APPROVED BY: JJ

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS | INITIAL | CONSOLIDATED |
|--------------------------|---------|--------------|
| DIAMETER-AVERAGE         | MM      | 71.520       |
| LENGTH---AVERAGE         | MM      | 142.600      |
| AREA                     | CM2     | 40.174       |
| VOLUME                   | CM3     | 572.881      |
| WET DENSITY              | G/CM3   | 2.145        |
| DRY DENSITY              | G/CM3   | 1.909        |
| WATER CONTENT            | %       | 12.400       |

| TEST PARAMETERS FOR CONSOLIDATION |        |       |
|-----------------------------------|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 | 7.520 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 | 7.520 |
| BACK PRESSURE                     | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 | 3.520 |
| EFFECTIVE SIGMA 3                 | KG/CM2 | 3.520 |
| CONSOLIDATION RATIO               |        | 1.000 |
| STRAIN RATE                       | MM/MIN | 0.100 |

BORING:  
 SAMPLE: 3  
 DEPTH: 38-39

STS JOB NO: 25331  
 EFF. SIGMA3: 3.520 KG/CM2

TEST RESULTS-----

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P      | PBAR   | Q OR   | A      |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| KG    | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |
| 0.0   | 0.00  | 3786. | 0.00   | 3.52   | 3.52   | 3.52   | 3.52   | 0.0    | 0.00   | 1.00   | 3.52   | 3.52   | 0.00   | 0.00   |
| 11.7  | 0.06  | 3798. | 0.13   | 3.83   | 3.52   | 3.70   | 3.39   | 0.0    | 0.31   | 1.09   | 3.67   | 3.54   | 0.15   | 0.43   |
| 26.2  | 0.14  | 3790. | 0.40   | 4.21   | 3.52   | 3.81   | 3.12   | 0.1    | 0.69   | 1.22   | 3.87   | 3.47   | 0.35   | 0.57   |
| 42.2  | 0.28  | 3794. | 0.72   | 4.63   | 3.52   | 3.91   | 2.80   | 0.2    | 1.11   | 1.40   | 4.08   | 3.36   | 0.56   | 0.65   |
| 52.4  | 0.38  | 3797. | 0.97   | 4.90   | 3.52   | 3.94   | 2.55   | 0.3    | 1.38   | 1.54   | 4.21   | 3.25   | 0.69   | 0.70   |
| 59.7  | 0.61  | 3803. | 1.14   | 5.09   | 3.52   | 3.95   | 2.38   | 0.4    | 1.57   | 1.66   | 4.30   | 3.17   | 0.78   | 0.72   |
| 64.1  | 0.69  | 3805. | 1.21   | 5.20   | 3.52   | 3.99   | 2.31   | 0.5    | 1.68   | 1.73   | 4.36   | 3.15   | 0.84   | 0.72   |
| 67.0  | 0.87  | 3810. | 1.31   | 5.28   | 3.52   | 3.97   | 2.21   | 0.6    | 1.76   | 1.79   | 4.40   | 3.09   | 0.88   | 0.74   |
| 71.4  | 1.01  | 3814. | 1.40   | 5.39   | 3.52   | 3.99   | 2.12   | 0.7    | 1.87   | 1.88   | 4.46   | 3.06   | 0.94   | 0.75   |
| 74.3  | 1.23  | 3820. | 1.46   | 5.46   | 3.52   | 4.01   | 2.06   | 0.9    | 1.94   | 1.94   | 4.49   | 3.04   | 0.97   | 0.75   |
| 77.2  | 1.33  | 3823. | 1.50   | 5.54   | 3.52   | 4.04   | 2.02   | 1.0    | 2.02   | 2.00   | 4.53   | 3.03   | 1.01   | 0.74   |
| 78.7  | 1.45  | 3826. | 1.53   | 5.58   | 3.52   | 4.04   | 1.99   | 1.0    | 2.06   | 2.03   | 4.55   | 3.02   | 1.03   | 0.75   |
| 81.6  | 1.67  | 3832. | 1.57   | 5.65   | 3.52   | 4.08   | 1.95   | 1.2    | 2.13   | 2.09   | 4.58   | 3.01   | 1.06   | 0.74   |
| 84.5  | 1.93  | 3840. | 1.65   | 5.72   | 3.52   | 4.07   | 1.87   | 1.4    | 2.20   | 2.17   | 4.62   | 2.97   | 1.10   | 0.75   |
| 87.4  | 2.20  | 3847. | 1.67   | 5.79   | 3.52   | 4.13   | 1.85   | 1.6    | 2.27   | 2.22   | 4.66   | 2.99   | 1.14   | 0.73   |
| 91.8  | 2.58  | 3858. | 1.68   | 5.90   | 3.52   | 4.22   | 1.84   | 1.9    | 2.38   | 2.30   | 4.71   | 3.03   | 1.19   | 0.71   |
| 93.2  | 2.80  | 3864. | 1.68   | 5.93   | 3.52   | 4.25   | 1.84   | 2.0    | 2.41   | 2.31   | 4.73   | 3.04   | 1.21   | 0.70   |
| 94.7  | 3.20  | 3876. | 1.70   | 5.96   | 3.52   | 4.26   | 1.82   | 2.3    | 2.44   | 2.34   | 4.74   | 3.04   | 1.22   | 0.70   |
| 96.1  | 3.65  | 3889. | 1.68   | 5.99   | 3.52   | 4.31   | 1.84   | 2.6    | 2.47   | 2.35   | 4.76   | 3.07   | 1.24   | 0.68   |
| 99.0  | 4.05  | 3900. | 1.68   | 6.06   | 3.52   | 4.37   | 1.84   | 2.9    | 2.54   | 2.38   | 4.79   | 3.11   | 1.27   | 0.66   |
| 100.5 | 4.65  | 3918. | 1.63   | 6.09   | 3.52   | 4.46   | 1.89   | 3.3    | 2.57   | 2.36   | 4.80   | 3.18   | 1.28   | 0.63   |
| 100.5 | 5.28  | 3936. | 1.63   | 6.07   | 3.52   | 4.45   | 1.89   | 3.8    | 2.55   | 2.35   | 4.80   | 3.17   | 1.28   | 0.64   |
| 102.0 | 5.92  | 3955. | 1.57   | 6.10   | 3.52   | 4.53   | 1.95   | 4.3    | 2.58   | 2.32   | 4.81   | 3.24   | 1.29   | 0.61   |
| 103.4 | 6.73  | 3979. | 1.55   | 6.12   | 3.52   | 4.57   | 1.97   | 4.8    | 2.60   | 2.32   | 4.82   | 3.27   | 1.30   | 0.60   |
| 104.9 | 7.23  | 3994. | 1.51   | 6.15   | 3.52   | 4.63   | 2.01   | 5.2    | 2.63   | 2.31   | 4.83   | 3.32   | 1.31   | 0.58   |
| 104.9 | 7.84  | 4013. | 1.51   | 6.13   | 3.52   | 4.62   | 2.01   | 5.6    | 2.61   | 2.30   | 4.83   | 3.31   | 1.31   | 0.58   |
| 106.3 | 8.26  | 4026. | 1.50   | 6.16   | 3.52   | 4.67   | 2.02   | 5.9    | 2.64   | 2.30   | 4.84   | 3.35   | 1.32   | 0.57   |
| 107.8 | 8.88  | 4045. | 1.50   | 6.19   | 3.52   | 4.69   | 2.02   | 6.4    | 2.67   | 2.32   | 4.85   | 3.36   | 1.33   | 0.56   |
| 107.8 | 9.29  | 4058. | 1.48   | 6.18   | 3.52   | 4.70   | 2.04   | 6.7    | 2.66   | 2.30   | 4.85   | 3.37   | 1.33   | 0.56   |
| 109.2 | 9.91  | 4077. | 1.48   | 6.20   | 3.52   | 4.72   | 2.04   | 7.1    | 2.68   | 2.31   | 4.86   | 3.38   | 1.34   | 0.55   |
| 110.7 | 10.47 | 4095. | 1.42   | 6.22   | 3.52   | 4.80   | 2.10   | 7.5    | 2.70   | 2.29   | 4.87   | 3.45   | 1.35   | 0.52   |
| 112.2 | 11.00 | 4112. | 1.44   | 6.25   | 3.52   | 4.81   | 2.08   | 7.9    | 2.73   | 2.31   | 4.88   | 3.45   | 1.36   | 0.53   |
| 116.5 | 11.92 | 4142. | 1.42   | 6.33   | 3.52   | 4.91   | 2.10   | 8.6    | 2.81   | 2.34   | 4.93   | 3.51   | 1.41   | 0.50   |
| 118.0 | 12.49 | 4160. | 1.38   | 6.36   | 3.52   | 4.98   | 2.14   | 9.0    | 2.84   | 2.33   | 4.94   | 3.56   | 1.42   | 0.49   |
| 119.4 | 13.11 | 4181. | 1.38   | 6.38   | 3.52   | 4.99   | 2.14   | 9.4    | 2.86   | 2.34   | 4.95   | 3.57   | 1.43   | 0.48   |
| 120.9 | 13.74 | 4202. | 1.32   | 6.40   | 3.52   | 5.07   | 2.20   | 9.9    | 2.88   | 2.31   | 4.96   | 3.63   | 1.44   | 0.46   |
| 122.4 | 14.36 | 4223. | 1.34   | 6.42   | 3.52   | 5.08   | 2.18   | 10.3   | 2.90   | 2.33   | 4.97   | 3.63   | 1.45   | 0.46   |
| 123.8 | 14.99 | 4244. | 1.31   | 6.44   | 3.52   | 5.13   | 2.21   | 10.8   | 2.92   | 2.32   | 4.98   | 3.67   | 1.46   | 0.45   |
| 126.7 | 15.61 | 4266. | 1.29   | 6.49   | 3.52   | 5.20   | 2.23   | 11.2   | 2.97   | 2.33   | 5.01   | 3.72   | 1.49   | 0.43   |
| 129.6 | 16.21 | 4286. | 1.29   | 6.54   | 3.52   | 5.26   | 2.23   | 11.7   | 3.02   | 2.35   | 5.03   | 3.74   | 1.51   | 0.43   |
| 132.5 | 16.84 | 4309. | 1.23   | 6.60   | 3.52   | 5.37   | 2.29   | 12.1   | 3.08   | 2.34   | 5.06   | 3.83   | 1.54   | 0.40   |
| 134.0 | 17.48 | 4331. | 1.23   | 6.61   | 3.52   | 5.38   | 2.29   | 12.6   | 3.09   | 2.35   | 5.07   | 3.84   | 1.55   | 0.40   |
| 136.9 | 18.05 | 4352. | 1.17   | 6.67   | 3.52   | 5.49   | 2.35   | 13.0   | 3.15   | 2.34   | 5.09   | 3.92   | 1.57   | 0.37   |
| 139.8 | 18.73 | 4376. | 1.17   | 6.71   | 3.52   | 5.54   | 2.35   | 13.5   | 3.19   | 2.36   | 5.12   | 3.94   | 1.60   | 0.37   |
| 139.8 | 19.36 | 4399. | 1.15   | 6.70   | 3.52   | 5.54   | 2.37   | 13.9   | 3.18   | 2.34   | 5.11   | 3.96   | 1.59   | 0.36   |
| 144.2 | 19.96 | 4421. | 1.12   | 6.78   | 3.52   | 5.67   | 2.40   | 14.4   | 3.26   | 2.36   | 5.15   | 4.03   | 1.63   | 0.34   |
| 147.1 | 20.61 | 4446. | 1.10   | 6.83   | 3.52   | 5.73   | 2.42   | 14.8   | 3.31   | 2.37   | 5.17   | 4.08   | 1.65   | 0.33   |

TEST RESULTS-----CONTINUED FROM PREVIOUS PAGE-----

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P      | PBAR   | Q OR   | A      |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| KG    | MM    | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | %      | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |
| 160.2 | 22.26 | 4509. | 0.98   | 7.07   | 3.52   | 6.09   | 2.54   | 16.0   | 3.55   | 2.40   | 5.30   | 4.31   | 1.78   | 0.28   |
| 163.1 | 22.88 | 4533. | 0.91   | 7.12   | 3.52   | 6.21   | 2.61   | 16.5   | 3.60   | 2.38   | 5.32   | 4.41   | 1.30   | 0.25   |
| 163.1 | 23.79 | 4568. | 0.85   | 7.09   | 3.52   | 6.24   | 2.67   | 17.1   | 3.57   | 2.34   | 5.31   | 4.45   | 1.79   | 0.24   |
| 169.0 | 24.71 | 4605. | 0.81   | 7.19   | 3.52   | 6.38   | 2.71   | 17.8   | 3.67   | 2.36   | 5.35   | 4.54   | 1.33   | 0.22   |
| 174.8 | 25.72 | 4646. | 0.76   | 7.28   | 3.52   | 6.53   | 2.76   | 18.5   | 3.76   | 2.36   | 5.40   | 4.64   | 1.88   | 0.20   |
| 180.6 | 26.67 | 4686. | 0.72   | 7.37   | 3.52   | 6.66   | 2.80   | 19.2   | 3.85   | 2.38   | 5.45   | 4.73   | 1.93   | 0.19   |
| 182.1 | 27.27 | 4711. | 0.66   | 7.39   | 3.52   | 6.72   | 2.86   | 19.6   | 3.87   | 2.35   | 5.45   | 4.79   | 1.93   | 0.17   |
| 182.1 | 27.94 | 4735. | 0.62   | 7.37   | 3.52   | 6.74   | 2.90   | 20.0   | 3.85   | 2.33   | 5.44   | 4.82   | 1.92   | 0.16   |





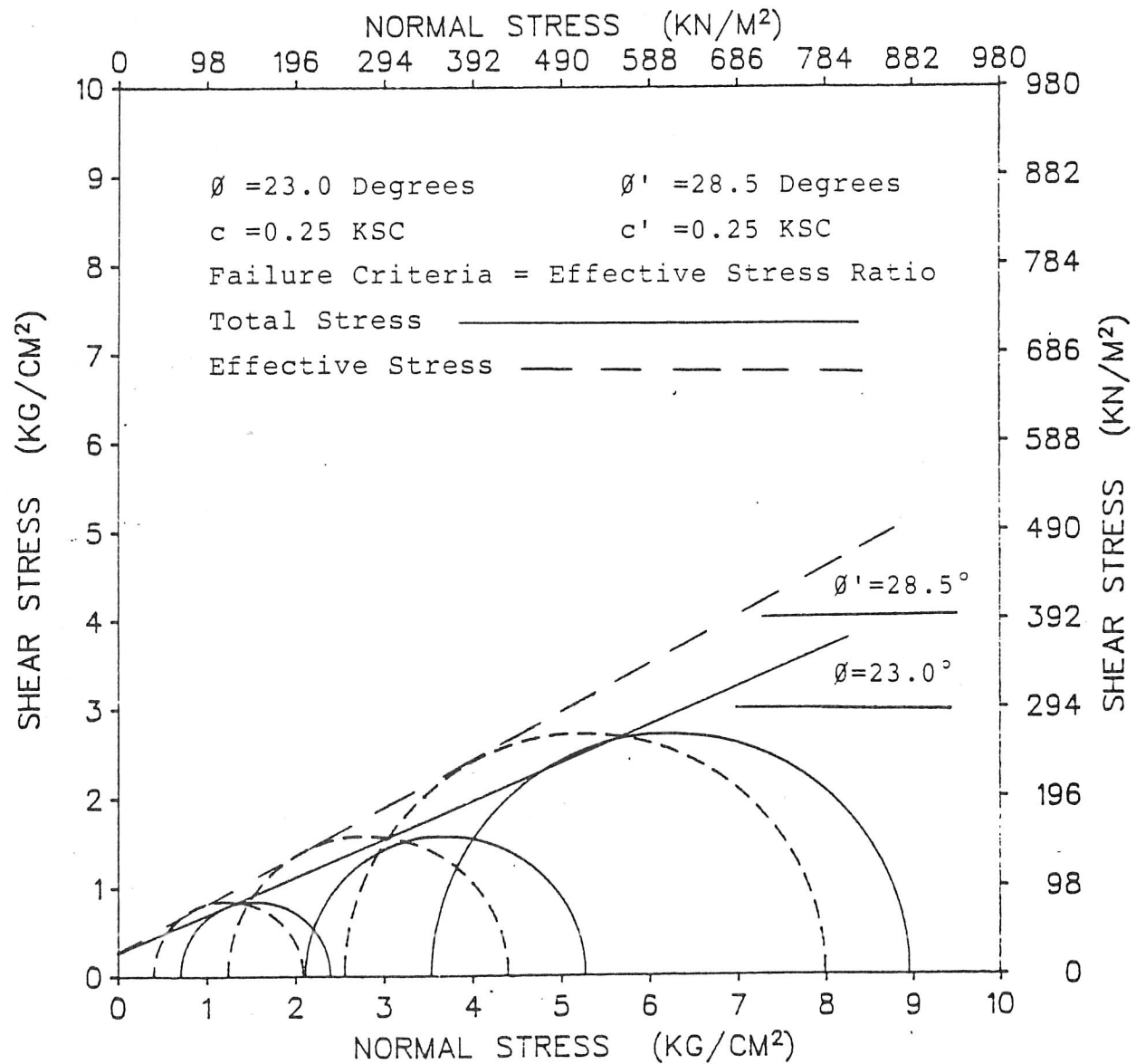
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |             |              |
|-------------|-------------|--------------|
| Boring: S-5 | Sample: SS4 | Depth: 18-20 |
| Boring: S-5 | Sample: SS6 | Depth: 22-24 |
| Boring: S-5 | Sample: SS4 | Depth: 25-27 |

MOHR ENVELOPE



Sigma 3 = 0.7 ksc  
 Sigma 3 = 2.1 ksc  
 Sigma 3 = 3.5 ksc

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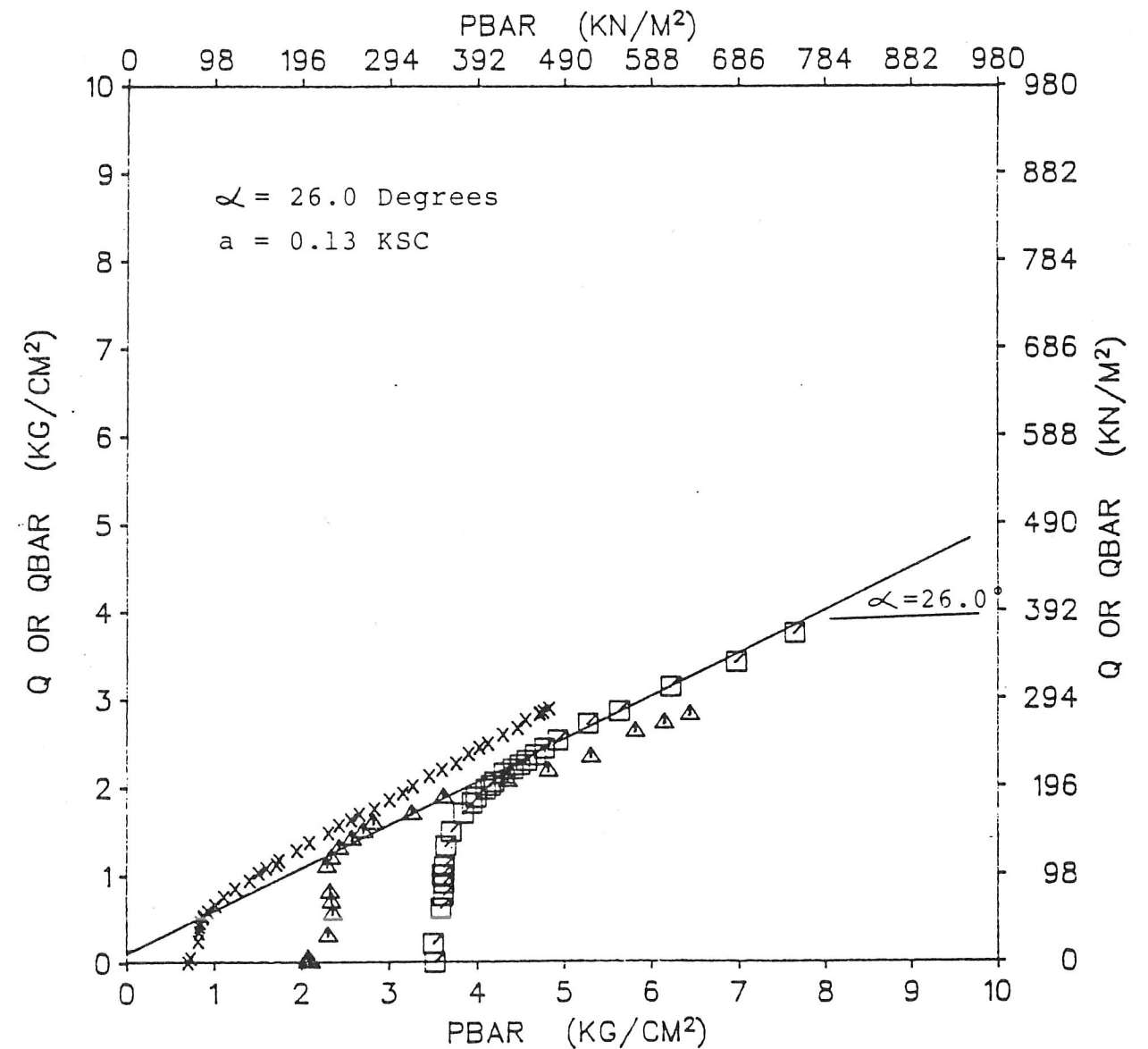
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |             |              |
|-------------|-------------|--------------|
| Boring: S-5 | Sample: SS4 | Depth: 18-20 |
| Boring: S-5 | Sample: SS6 | Depth: 22-24 |
| Boring: S-5 | Sample: SS4 | Depth: 25-27 |

STRESS PATH PLOT



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 2.1 ksc  
 □ Sigma 3 = 3.5 ksc

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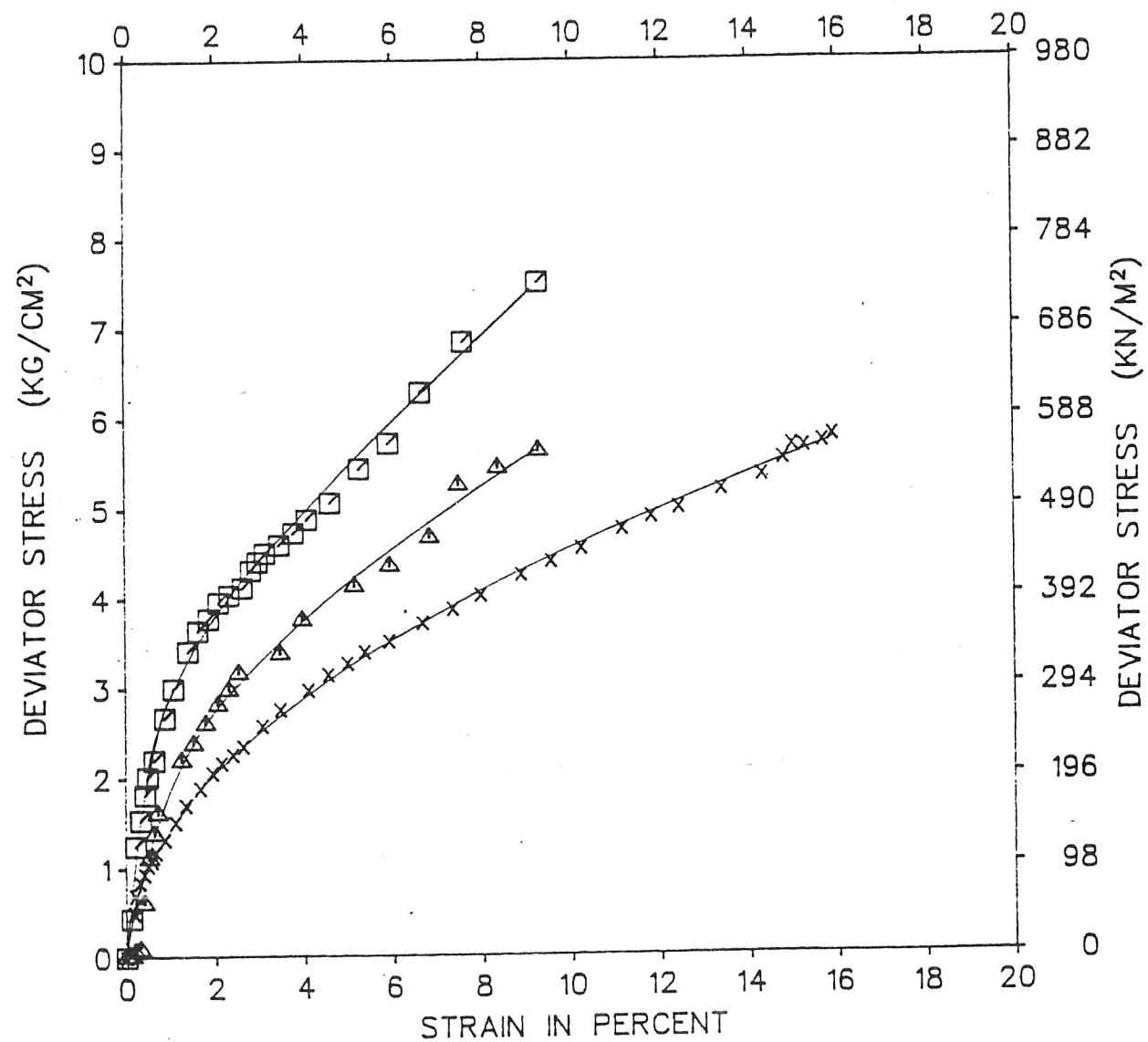
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |             |              |
|-------------|-------------|--------------|
| Boring: S-5 | Sample: SS4 | Depth: 18-20 |
| Boring: S-5 | Sample: SS6 | Depth: 22-24 |
| Boring: S-5 | Sample: SS4 | Depth: 25-27 |

DEVIATOR STRESS vs STRAIN



- x Sigma 3 = 0.7 ksc
- △ Sigma 3 = 2.1 ksc
- Sigma 3 = 3.5 ksc

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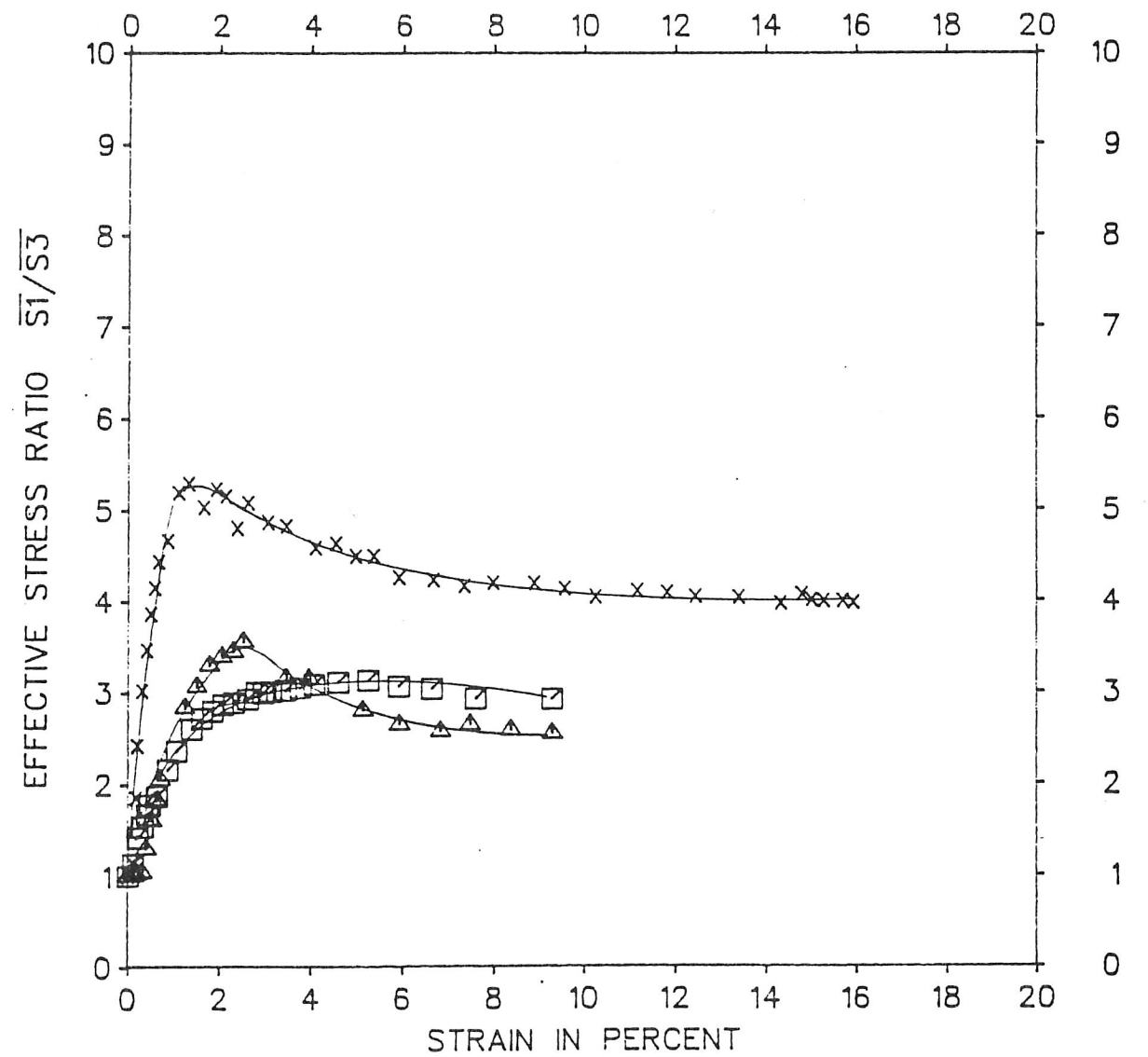
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |             |              |
|-------------|-------------|--------------|
| Boring: S-5 | Sample: SS4 | Depth: 18-20 |
| Boring: S-5 | Sample: SS6 | Depth: 22-24 |
| Boring: S-5 | Sample: SS4 | Depth: 25-27 |

EFFECTIVE STRESS RATIO vs STRAIN



- x Sigma 3 = 0.7 ksc
- △ Sigma 3 = 2.1 ksc
- Sigma 3 = 3.5 ksc

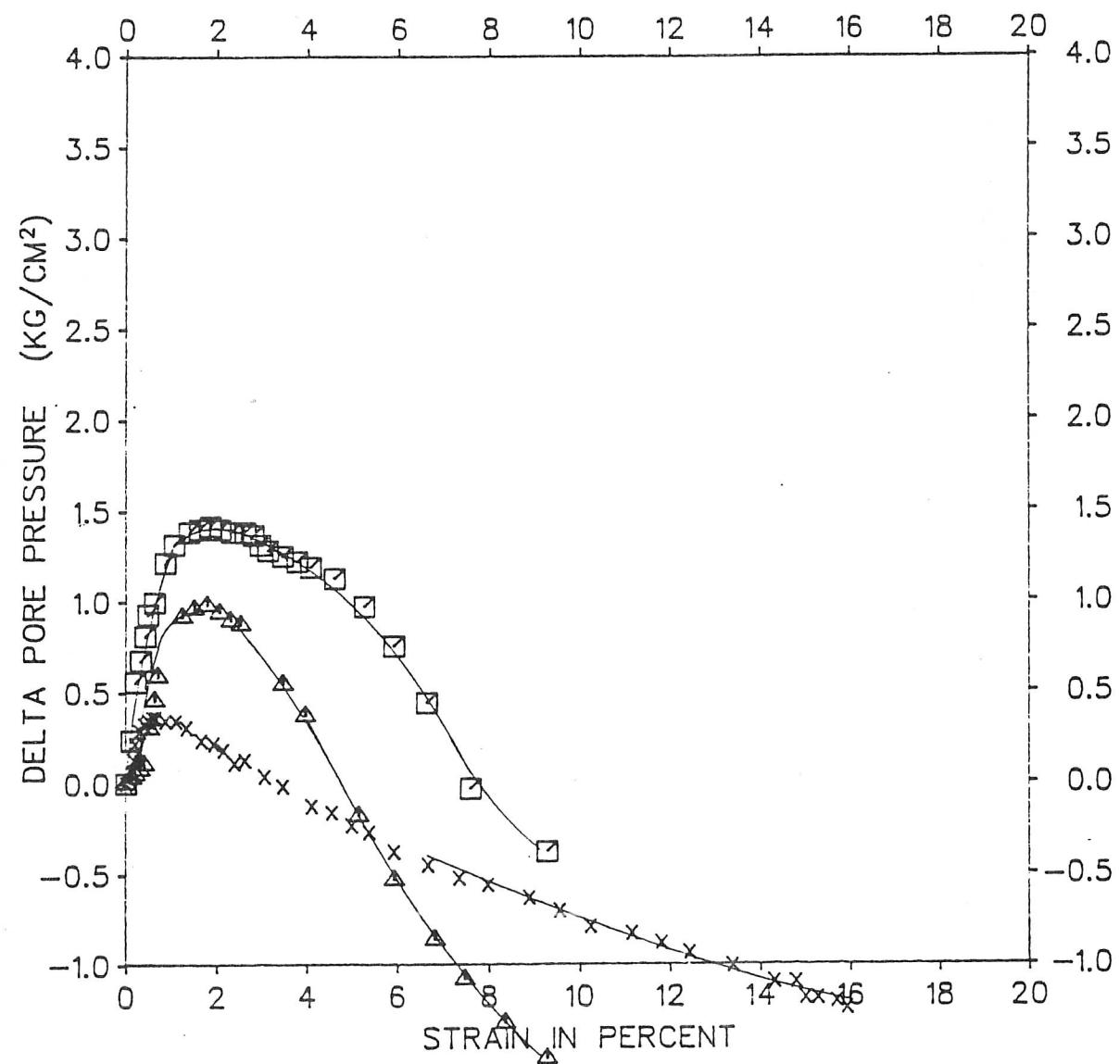
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STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |             |              |
|-------------|-------------|--------------|
| Boring: S-5 | Sample: SS4 | Depth: 18-20 |
| Boring: S-5 | Sample: SS6 | Depth: 22-24 |
| Boring: S-5 | Sample: SS4 | Depth: 25-27 |

DELTA PORE PRESSURE vs STRAIN



$\times$  Sigma 3 = 0.7 ksc  
 $\triangle$  Sigma 3 = 2.1 ksc  
 $\square$  Sigma 3 = 3.5 ksc

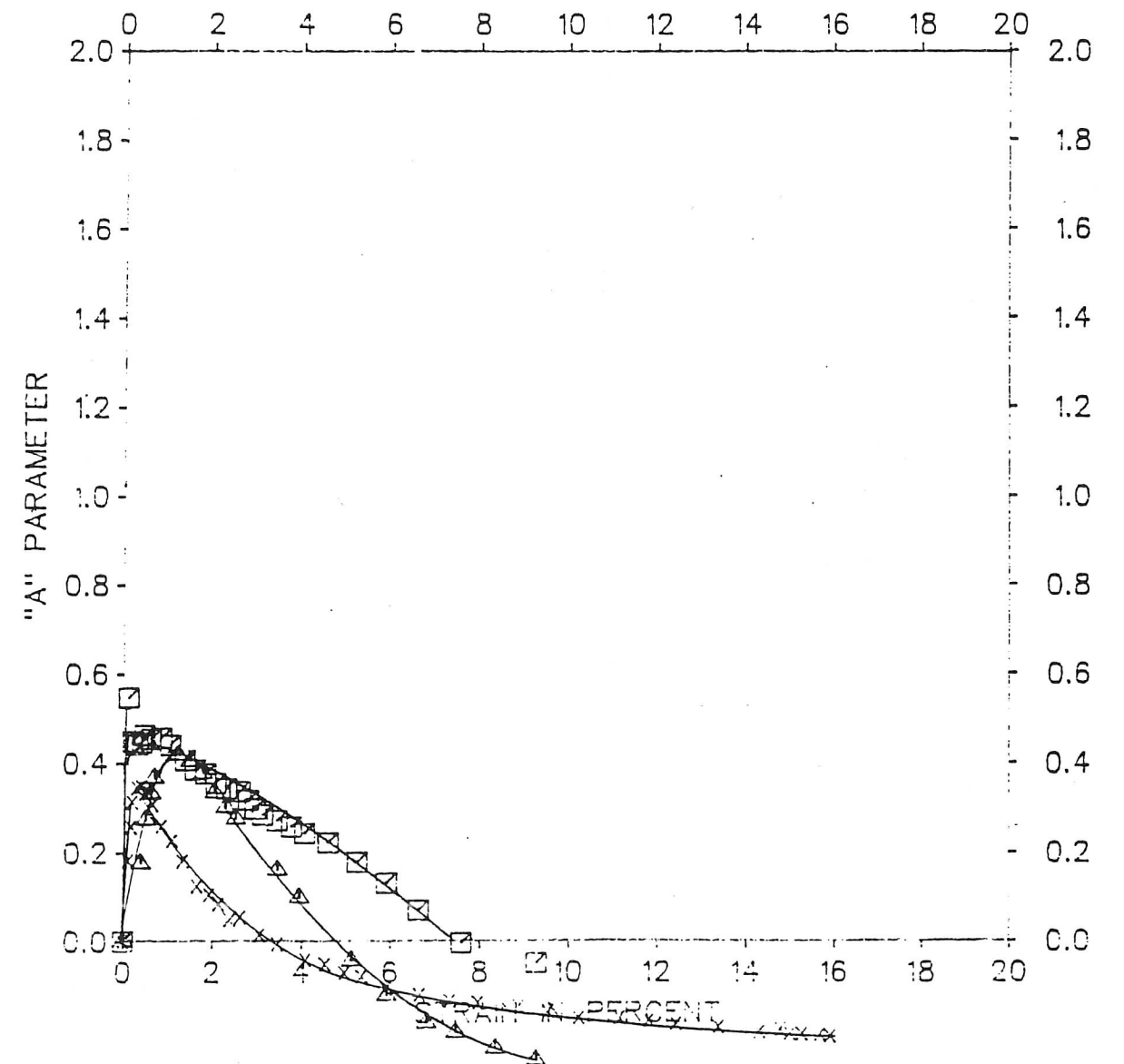
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STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|             |             |              |
|-------------|-------------|--------------|
| Boring: S-5 | Sample: SS4 | Depth: 18-20 |
| Boring: S-5 | Sample: SS6 | Depth: 22-24 |
| Boring: S-5 | Sample: SS4 | Depth: 25-27 |

"A" PARAMETER vs STRAIN



$\times$  Sigma 3 = 0.7 ksc  
 $\triangle$  Sigma 3 = 2.1 ksc  
 $\square$  Sigma 3 = 3.5 ksc

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STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
BORING: 3-5  
SAMPLE: SS4  
DEPTH: 13-20

STS JOB NO: 25331  
DATE: 3-1-88  
TESTED BY: JJ  
APPROVED BY: WFD

SOIL DESC: Silty Sand trace Fine Gravel trace  
Clay - Reddish Brown (SM)

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS |       | INITIAL | CONSOLIDATED |
|--------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE         | MM    | 63.210  | 63.035       |
| LENGTH-AVERAGE           | MM    | 139.080 | 138.960      |
| AREA                     | CM2   | 31.381  | 31.207       |
| VOLUME                   | CM3   | 436.442 | 433.652      |
| WET DENSITY              | G/CM3 | 2.285   | 2.308        |
| DRY DENSITY              | G/CM3 | 2.070   | 2.083        |
| WATER CONTENT            | %     | 10.400  | 10.800       |

| TEST PARAMETERS FOR CONSOLIDATION |        |  |       |
|-----------------------------------|--------|--|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 |  | 4.700 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 |  | 4.700 |
| BACK PRESSURE                     | KG/CM2 |  | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 |  | 0.700 |
| EFFECTIVE SIGMA 3                 | KG/CM2 |  | 0.700 |
| CONSOLIDATION RATIO               |        |  | 1.000 |
| STRAIN RATE                       | MM/MIN |  | 0.100 |

BORING: 3-5  
SAMPLE: SS4  
DEPTH: 13-20

STS JOB NO: 25331  
EFF. SIGMA3: 0.700 KG/CM2

TEST RESULTS

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 - | S1BAR/ | P      | PEAR   | Q OR   | A      |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| KG    | MM    | MM2   | P.W.P. | TOTAL  | TOTAL  | BAR    | BAR    | %      | S3   | S3BAR  | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |
| 0.0   | 0.00  | 3121. | 0.00   | 0.70   | 0.70   | 0.70   | 0.70   | 0.0    | 0.00 | 1.00   | 0.70   | 0.70   | 0.00   | 0.00   |
| 3.1   | 0.14  | 3124. | 0.02   | 0.80   | 0.70   | 0.78   | 0.68   | 0.1    | 0.10 | 1.15   | 0.75   | 0.73   | 0.05   | 0.18   |
| 15.3  | 0.24  | 3126. | 0.13   | 1.19   | 0.70   | 1.06   | 0.57   | 0.2    | 0.49 | 1.85   | 0.94   | 0.82   | 0.24   | 0.26   |
| 21.5  | 0.28  | 3127. | 0.22   | 1.39   | 0.70   | 1.17   | 0.48   | 0.2    | 0.69 | 2.42   | 1.04   | 0.83   | 0.34   | 0.31   |
| 26.1  | 0.42  | 3130. | 0.29   | 1.53   | 0.70   | 1.25   | 0.41   | 0.3    | 0.83 | 3.02   | 1.12   | 0.83   | 0.42   | 0.34   |
| 29.1  | 0.56  | 3133. | 0.32   | 1.63   | 0.70   | 1.31   | 0.38   | 0.4    | 0.93 | 3.46   | 1.16   | 0.84   | 0.46   | 0.35   |
| 32.2  | 0.68  | 3136. | 0.34   | 1.73   | 0.70   | 1.39   | 0.36   | 0.5    | 1.03 | 3.86   | 1.21   | 0.87   | 0.51   | 0.33   |
| 33.7  | 0.80  | 3139. | 0.36   | 1.77   | 0.70   | 1.41   | 0.34   | 0.6    | 1.07 | 4.15   | 1.24   | 0.88   | 0.54   | 0.33   |
| 36.8  | 0.92  | 3141. | 0.36   | 1.87   | 0.70   | 1.51   | 0.34   | 0.7    | 1.17 | 4.44   | 1.29   | 0.93   | 0.59   | 0.31   |
| 41.4  | 1.20  | 3148. | 0.34   | 2.02   | 0.70   | 1.67   | 0.36   | 0.9    | 1.32 | 4.66   | 1.36   | 1.02   | 0.66   | 0.26   |
| 47.5  | 1.53  | 3155. | 0.34   | 2.21   | 0.70   | 1.86   | 0.36   | 1.1    | 1.51 | 5.19   | 1.45   | 1.11   | 0.75   | 0.23   |
| 53.6  | 1.85  | 3163. | 0.30   | 2.39   | 0.70   | 2.09   | 0.39   | 1.3    | 1.69 | 5.29   | 1.55   | 1.24   | 0.85   | 0.18   |
| 59.7  | 2.31  | 3173. | 0.23   | 2.58   | 0.70   | 2.35   | 0.47   | 1.7    | 1.88 | 5.03   | 1.64   | 1.41   | 0.94   | 0.12   |
| 65.3  | 2.69  | 3182. | 0.22   | 2.75   | 0.70   | 2.54   | 0.48   | 1.9    | 2.05 | 5.23   | 1.73   | 1.51   | 1.03   | 0.10   |
| 68.9  | 2.99  | 3189. | 0.18   | 2.86   | 0.70   | 2.68   | 0.52   | 2.2    | 2.16 | 5.15   | 1.78   | 1.60   | 1.08   | 0.08   |
| 72.0  | 3.33  | 3197. | 0.11   | 2.95   | 0.70   | 2.84   | 0.59   | 2.4    | 2.25 | 4.80   | 1.83   | 1.72   | 1.13   | 0.05   |
| 75.1  | 3.66  | 3205. | 0.13   | 3.04   | 0.70   | 2.92   | 0.57   | 2.6    | 2.34 | 5.08   | 1.87   | 1.75   | 1.17   | 0.05   |
| 82.7  | 4.26  | 3219. | 0.04   | 3.27   | 0.70   | 3.23   | 0.66   | 3.1    | 2.57 | 4.87   | 1.98   | 1.95   | 1.28   | 0.01   |
| 88.9  | 4.82  | 3233. | -0.02  | 3.45   | 0.70   | 3.47   | 0.72   | 3.5    | 2.75 | 4.83   | 2.07   | 2.09   | 1.37   | -0.01  |
| 96.5  | 5.70  | 3254. | -0.13  | 3.67   | 0.70   | 3.79   | 0.83   | 4.1    | 2.97 | 4.59   | 2.18   | 2.31   | 1.48   | -0.04  |
| 102.6 | 6.33  | 3270. | -0.16  | 3.84   | 0.70   | 4.00   | 0.86   | 4.6    | 3.14 | 4.64   | 2.27   | 2.43   | 1.57   | -0.05  |
| 107.2 | 6.93  | 3284. | -0.23  | 3.96   | 0.70   | 4.20   | 0.93   | 5.0    | 3.26 | 4.49   | 2.33   | 2.57   | 1.63   | -0.07  |
| 111.8 | 7.47  | 3298. | -0.27  | 4.09   | 0.70   | 4.36   | 0.97   | 5.4    | 3.39 | 4.50   | 2.39   | 2.66   | 1.69   | -0.08  |
| 116.4 | 8.23  | 3317. | -0.38  | 4.21   | 0.70   | 4.59   | 1.08   | 5.9    | 3.51 | 4.26   | 2.45   | 2.83   | 1.75   | -0.11  |
| 124.1 | 9.26  | 3344. | -0.45  | 4.41   | 0.70   | 4.86   | 1.15   | 6.7    | 3.71 | 4.23   | 2.56   | 3.00   | 1.86   | -0.12  |
| 130.2 | 10.20 | 3368. | -0.52  | 4.57   | 0.70   | 5.09   | 1.22   | 7.3    | 3.87 | 4.17   | 2.63   | 3.15   | 1.93   | -0.13  |
| 136.3 | 11.09 | 3391. | -0.56  | 4.72   | 0.70   | 5.28   | 1.26   | 8.0    | 4.02 | 4.20   | 2.71   | 3.27   | 2.01   | -0.14  |
| 145.5 | 12.35 | 3425. | -0.63  | 4.95   | 0.70   | 5.58   | 1.33   | 8.9    | 4.25 | 4.20   | 2.82   | 3.45   | 2.12   | -0.15  |
| 151.7 | 13.29 | 3451. | -0.70  | 5.10   | 0.70   | 5.80   | 1.40   | 9.6    | 4.40 | 4.14   | 2.90   | 3.60   | 2.20   | -0.16  |
| 157.8 | 14.24 | 3477. | -0.79  | 5.24   | 0.70   | 6.03   | 1.49   | 10.2   | 4.54 | 4.05   | 2.97   | 3.76   | 2.27   | -0.17  |
| 167.0 | 15.52 | 3513. | -0.83  | 5.45   | 0.70   | 6.28   | 1.53   | 11.2   | 4.75 | 4.12   | 3.08   | 3.90   | 2.38   | -0.17  |
| 173.1 | 16.43 | 3539. | -0.88  | 5.59   | 0.70   | 6.47   | 1.58   | 11.8   | 4.89 | 4.10   | 3.15   | 4.03   | 2.45   | -0.18  |
| 177.7 | 17.29 | 3564. | -0.93  | 5.69   | 0.70   | 6.62   | 1.63   | 12.4   | 4.99 | 4.05   | 3.19   | 4.13   | 2.49   | -0.19  |
| 186.9 | 18.62 | 3604. | -1.01  | 5.89   | 0.70   | 6.89   | 1.71   | 13.4   | 5.19 | 4.04   | 3.29   | 4.30   | 2.59   | -0.19  |
| 194.5 | 19.90 | 3642. | -1.10  | 6.04   | 0.70   | 7.14   | 1.80   | 14.3   | 5.34 | 3.97   | 3.37   | 4.47   | 2.67   | -0.21  |
| 202.2 | 20.56 | 3663. | -1.10  | 6.22   | 0.70   | 7.32   | 1.80   | 14.8   | 5.52 | 4.07   | 3.46   | 4.56   | 2.76   | -0.20  |
| 208.3 | 20.85 | 3672. | -1.18  | 6.37   | 0.70   | 7.56   | 1.88   | 15.0   | 5.67 | 4.01   | 3.54   | 4.72   | 2.84   | -0.21  |
| 208.3 | 21.23 | 3683. | -1.18  | 6.36   | 0.70   | 7.54   | 1.88   | 15.3   | 5.66 | 4.00   | 3.53   | 4.71   | 2.83   | -0.21  |
| 211.4 | 21.81 | 3702. | -1.20  | 6.41   | 0.70   | 7.61   | 1.90   | 15.7   | 5.71 | 4.00   | 3.56   | 4.76   | 2.86   | -0.21  |
| 214.5 | 22.13 | 3712. | -1.24  | 6.48   | 0.70   | 7.72   | 1.94   | 15.9   | 5.78 | 3.98   | 3.59   | 4.83   | 2.89   | -0.21  |

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TRIAxIAL COMPRESSION TEST  
CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
BORING: 8-5  
SAMPLE: 886  
DEPTH: 22-24

STS JOB NO: 25331  
DATE: 3-1-88  
TESTED BY: JJ  
APPROVED BY: JJS

SOIL DESC: Silty Sand trace Fine Gravel trace  
Clay - Reddish Brown (SM)

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS |       | INITIAL | CONSOLIDATED |
|--------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE         | MM    | 64.240  | 63.515       |
| LENGTH---AVERAGE         | MM    | 138.120 | 137.900      |
| AREA                     | CM2   | 32.412  | 31.684       |
| VOLUME                   | CM3   | 447.669 | 436.923      |
| WET DENSITY              | G/CM3 | 2.251   | 2.319        |
| DRY DENSITY              | G/CM3 | 2.065   | 2.116        |
| WATER CONTENT            | %     | 9.000   | 9.600        |

| TEST PARAMETERS FOR CONSOLIDATION |        |       |
|-----------------------------------|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 | 6.110 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 | 6.110 |
| BACK PRESSURE                     | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 | 2.110 |
| EFFECTIVE SIGMA 3                 | KG/CM2 | 2.110 |
| CONSOLIDATION RATIO               |        | 1.000 |
| STRAIN RATE                       | MM/MIN | 0.100 |

BORING: 8-5  
SAMPLE: 886  
DEPTH: 22-24

STS JOB NO: 25331  
EFF. SIGMA3: 2.110 KG/CM2

TEST RESULTS

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 - | S1BAR/ | P      | PBAR   | U OR   | A     |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|-------|
| KG    | MM    | MM2   | P.W.P. | TOTAL  | TOTAL  | BAR    | BAR    | %      | S3   | S3BAR  | KG/CM2 | KG/CM2 | KG/CM2 |       |
| 0.0   | 0.00  | 3168. | 0.00   | 2.11   | 2.11   | 2.11   | 2.11   | 0.0    | 0.00 | 1.00   | 2.11   | 2.11   | 0.00   | 0.00  |
| 1.6   | 0.28  | 3175. | 0.05   | 2.16   | 2.11   | 2.11   | 2.06   | 0.2    | 0.05 | 1.02   | 2.14   | 2.08   | 0.03   | 1.33  |
| 2.6   | 0.43  | 3178. | 0.08   | 2.19   | 2.11   | 2.12   | 2.03   | 0.3    | 0.08 | 1.04   | 2.15   | 2.07   | 0.04   | 0.93  |
| 19.1  | 0.55  | 3181. | 0.11   | 2.71   | 2.11   | 2.61   | 2.01   | 0.4    | 0.60 | 1.30   | 2.41   | 2.31   | 0.30   | 0.17  |
| 35.1  | 0.71  | 3185. | 0.30   | 3.21   | 2.11   | 2.91   | 1.81   | 0.5    | 1.10 | 1.61   | 2.66   | 2.36   | 0.55   | 0.27  |
| 43.8  | 0.87  | 3189. | 0.46   | 3.48   | 2.11   | 3.03   | 1.65   | 0.6    | 1.37 | 1.83   | 2.80   | 2.34   | 0.69   | 0.33  |
| 51.1  | 0.97  | 3191. | 0.59   | 3.71   | 2.11   | 3.12   | 1.52   | 0.7    | 1.60 | 2.05   | 2.91   | 2.32   | 0.80   | 0.37  |
| 70.2  | 1.71  | 3208. | 0.92   | 4.30   | 2.11   | 3.38   | 1.19   | 1.2    | 2.19 | 2.83   | 3.20   | 2.29   | 1.09   | 0.42  |
| 76.4  | 2.08  | 3217. | 0.96   | 4.48   | 2.11   | 3.52   | 1.15   | 1.5    | 2.37 | 3.07   | 3.30   | 2.34   | 1.19   | 0.40  |
| 83.8  | 2.46  | 3226. | 0.98   | 4.71   | 2.11   | 3.73   | 1.13   | 1.8    | 2.60 | 3.30   | 3.41   | 2.43   | 1.30   | 0.38  |
| 90.8  | 2.84  | 3235. | 0.94   | 4.92   | 2.11   | 3.98   | 1.17   | 2.1    | 2.81 | 3.39   | 3.51   | 2.58   | 1.40   | 0.33  |
| 96.5  | 3.18  | 3243. | 0.89   | 5.09   | 2.11   | 4.19   | 1.22   | 2.3    | 2.98 | 3.45   | 3.60   | 2.70   | 1.49   | 0.30  |
| 102.8 | 3.49  | 3251. | 0.87   | 5.27   | 2.11   | 4.40   | 1.24   | 2.5    | 3.16 | 3.55   | 3.69   | 2.82   | 1.58   | 0.28  |
| 110.8 | 4.78  | 3282. | 0.54   | 5.49   | 2.11   | 4.94   | 1.57   | 3.5    | 3.38 | 3.15   | 3.90   | 3.25   | 1.69   | 0.16  |
| 123.7 | 5.46  | 3299. | 0.37   | 5.86   | 2.11   | 5.49   | 1.74   | 4.0    | 3.75 | 3.15   | 3.98   | 3.62   | 1.87   | 0.10  |
| 137.8 | 7.09  | 3340. | -0.18  | 6.24   | 2.11   | 6.42   | 2.29   | 5.1    | 4.13 | 2.80   | 4.17   | 4.35   | 2.06   | -0.04 |
| 146.5 | 8.18  | 3368. | -0.53  | 6.46   | 2.11   | 6.99   | 2.64   | 5.9    | 4.35 | 2.65   | 4.28   | 4.82   | 2.17   | -0.12 |
| 158.7 | 9.41  | 3400. | -0.86  | 6.78   | 2.11   | 7.64   | 2.97   | 6.8    | 4.67 | 2.57   | 4.44   | 5.30   | 2.33   | -0.18 |
| 179.8 | 10.31 | 3424. | -1.08  | 7.36   | 2.11   | 8.44   | 3.19   | 7.5    | 5.25 | 2.65   | 4.74   | 5.82   | 2.63   | -0.21 |
| 188.0 | 11.54 | 3458. | -1.32  | 7.55   | 2.11   | 8.87   | 3.43   | 8.4    | 5.44 | 2.58   | 4.83   | 6.15   | 2.72   | -0.24 |
| 196.5 | 12.81 | 3493. | -1.52  | 7.74   | 2.11   | 9.25   | 3.63   | 9.3    | 5.63 | 2.55   | 4.92   | 6.44   | 2.81   | -0.27 |

STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
BORING: S-5  
SAMPLE: SS4  
DEPTH: 25-27  
SOIL DESC: Silty Sand trace Fine Gravel trace  
CLAY -- REDDISH BROWN (SM)

STS JOB NO: 25331  
DATE: 3-1-88  
TESTED BY: JJ  
APPROVED BY: MG

BORING: S-5  
SAMPLE: SS4  
DEPTH: 25-27

STS JOB NO: 25331  
EFF. SIGMA3: 3.520 KG/CM2

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS |       | INITIAL | CONSOLIDATED |
|--------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE         | MM    | 63.470  | 62.795       |
| LENGTH---AVERAGE         | MM    | 129.950 | 129.400      |
| AREA                     | CM2   | 31.639  | 30.970       |
| VOLUME                   | CM3   | 411.153 | 400.755      |
| WET DENSITY              | G/CM3 | 2.299   | 2.335        |
| DRY DENSITY              | G/CM3 | 2.084   | 2.138        |
| WATER CONTENT            | %     | 10.300  | 9.200        |

| TEST PARAMETERS FOR CONSOLIDATION |        |       |
|-----------------------------------|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 | 7.520 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 | 7.520 |
| BACK PRESSURE                     | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 | 3.520 |
| EFFECTIVE SIGMA 3                 | KG/CM2 | 3.520 |
| CONSOLIDATION RATIO               |        | 1.000 |
| STRAIN RATE                       | MM/MIN | 0.100 |

TEST RESULTS-----

| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 -   | S1BAR/ | P      | PBAR   | Q OR   | A     |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| KG    | MM    | AREA  | P.W.P. | TOTAL  | TOTAL  | BAR    | BAR    | %      | S3     | S3BAR  | KG/CM2 | KG/CM2 | DBAR   |       |
|       |       | MM2   | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |        | KG/CM2 |        |        |        | KG/CM2 |       |
| 0.0   | 0.00  | 3097. | 0.00   | 3.52   | 3.52   | 3.52   | 3.52   | 0.0    | 0.00   | 1.00   | 3.52   | 3.52   | 0.00   | 0.00  |
| 13.4  | 0.15  | 3101. | 0.24   | 3.95   | 3.52   | 3.72   | 3.28   | 0.1    | 0.43   | 1.13   | 3.74   | 3.50   | 0.22   | 0.55  |
| 38.6  | 0.27  | 3104. | 0.56   | 4.76   | 3.52   | 4.21   | 2.96   | 0.2    | 1.24   | 1.42   | 4.14   | 3.58   | 0.62   | 0.45  |
| 47.6  | 0.42  | 3107. | 0.68   | 5.05   | 3.52   | 4.38   | 2.84   | 0.3    | 1.53   | 1.54   | 4.29   | 3.61   | 0.77   | 0.44  |
| 56.5  | 0.54  | 3110. | 0.81   | 5.34   | 3.52   | 4.53   | 2.71   | 0.4    | 1.82   | 1.67   | 4.43   | 3.62   | 0.91   | 0.45  |
| 62.5  | 0.62  | 3112. | 0.93   | 5.53   | 3.52   | 4.60   | 2.59   | 0.5    | 2.01   | 1.77   | 4.52   | 3.60   | 1.00   | 0.46  |
| 68.4  | 0.81  | 3117. | 0.99   | 5.71   | 3.52   | 4.72   | 2.53   | 0.6    | 2.19   | 1.87   | 4.62   | 3.62   | 1.10   | 0.45  |
| 83.3  | 1.12  | 3124. | 1.22   | 6.19   | 3.52   | 4.97   | 2.30   | 0.9    | 2.67   | 2.16   | 4.95   | 3.64   | 1.33   | 0.46  |
| 93.7  | 1.37  | 3130. | 1.32   | 6.51   | 3.52   | 5.20   | 2.20   | 1.1    | 2.99   | 2.36   | 5.02   | 3.70   | 1.50   | 0.44  |
| 107.1 | 1.80  | 3141. | 1.38   | 6.93   | 3.52   | 5.55   | 2.14   | 1.4    | 3.41   | 2.60   | 5.23   | 3.84   | 1.71   | 0.41  |
| 114.5 | 2.09  | 3148. | 1.40   | 7.16   | 3.52   | 5.76   | 2.12   | 1.6    | 3.64   | 2.72   | 5.34   | 3.94   | 1.92   | 0.38  |
| 119.0 | 2.40  | 3156. | 1.42   | 7.29   | 3.52   | 5.87   | 2.10   | 1.9    | 3.77   | 2.79   | 5.41   | 3.99   | 1.89   | 0.38  |
| 125.0 | 2.69  | 3163. | 1.40   | 7.47   | 3.52   | 6.07   | 2.12   | 2.1    | 3.95   | 2.86   | 5.50   | 4.10   | 1.98   | 0.35  |
| 127.9 | 3.00  | 3171. | 1.38   | 7.55   | 3.52   | 6.17   | 2.14   | 2.3    | 4.03   | 2.89   | 5.54   | 4.15   | 2.02   | 0.34  |
| 130.9 | 3.39  | 3180. | 1.38   | 7.64   | 3.52   | 6.25   | 2.14   | 2.6    | 4.12   | 2.93   | 5.58   | 4.19   | 2.06   | 0.34  |
| 137.4 | 3.64  | 3187. | 1.37   | 7.83   | 3.52   | 6.46   | 2.15   | 2.8    | 4.31   | 3.00   | 5.68   | 4.31   | 2.16   | 0.32  |
| 140.6 | 3.83  | 3191. | 1.31   | 7.93   | 3.52   | 6.61   | 2.21   | 3.0    | 4.41   | 3.00   | 5.72   | 4.41   | 2.20   | 0.30  |
| 143.9 | 4.05  | 3197. | 1.28   | 8.02   | 3.52   | 6.74   | 2.24   | 3.1    | 4.50   | 3.01   | 5.77   | 4.49   | 2.25   | 0.28  |
| 147.4 | 4.47  | 3208. | 1.25   | 8.11   | 3.52   | 6.86   | 2.27   | 3.5    | 4.59   | 3.02   | 5.82   | 4.57   | 2.30   | 0.27  |
| 152.1 | 4.88  | 3218. | 1.22   | 8.25   | 3.52   | 7.03   | 2.30   | 3.8    | 4.73   | 3.05   | 5.98   | 4.66   | 2.36   | 0.26  |
| 157.4 | 5.27  | 3229. | 1.19   | 8.40   | 3.52   | 7.21   | 2.33   | 4.1    | 4.88   | 3.09   | 5.96   | 4.77   | 2.44   | 0.24  |
| 164.3 | 5.95  | 3246. | 1.13   | 8.58   | 3.52   | 7.46   | 2.39   | 4.6    | 5.06   | 3.11   | 6.05   | 4.93   | 2.53   | 0.22  |
| 177.8 | 6.80  | 3269. | 0.97   | 8.96   | 3.52   | 7.99   | 2.55   | 5.3    | 5.44   | 3.13   | 6.24   | 5.27   | 2.72   | 0.18  |
| 188.3 | 7.65  | 3292. | 0.75   | 9.24   | 3.52   | 8.49   | 2.77   | 5.9    | 5.72   | 3.07   | 6.38   | 5.63   | 2.86   | 0.13  |
| 208.3 | 8.58  | 3317. | 0.44   | 9.80   | 3.52   | 9.36   | 3.08   | 6.6    | 6.28   | 3.04   | 6.66   | 6.22   | 3.14   | 0.07  |
| 229.3 | 9.82  | 3351. | -0.03  | 10.36  | 3.52   | 10.39  | 3.55   | 7.6    | 6.84   | 2.93   | 6.94   | 6.97   | 3.42   | 0.00  |
| 256.1 | 12.01 | 3414. | -0.38  | 11.02  | 3.52   | 11.40  | 3.89   | 9.3    | 7.50   | 2.93   | 7.27   | 7.65   | 3.75   | -0.05 |



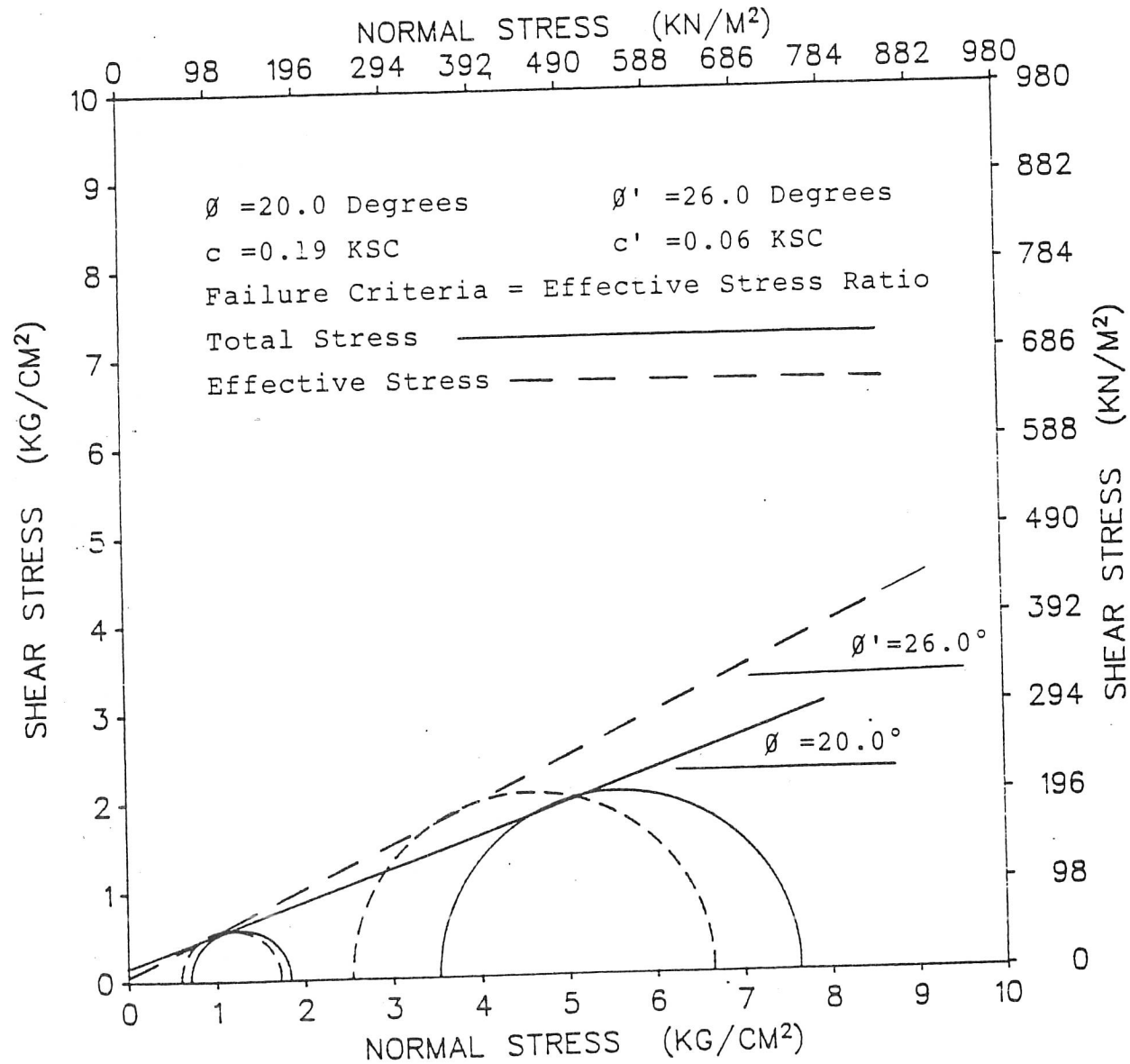
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|            |         |              |
|------------|---------|--------------|
| Boring: S5 | Sample: | Depth: 45-46 |
| Boring: S5 | Sample: | Depth: 46-47 |

MOHR ENVELOPE



$\sigma_3 = 0.7$  ksc  
 $\sigma_3 = 3.5$  ksc

BEST COPY AVAILABLE



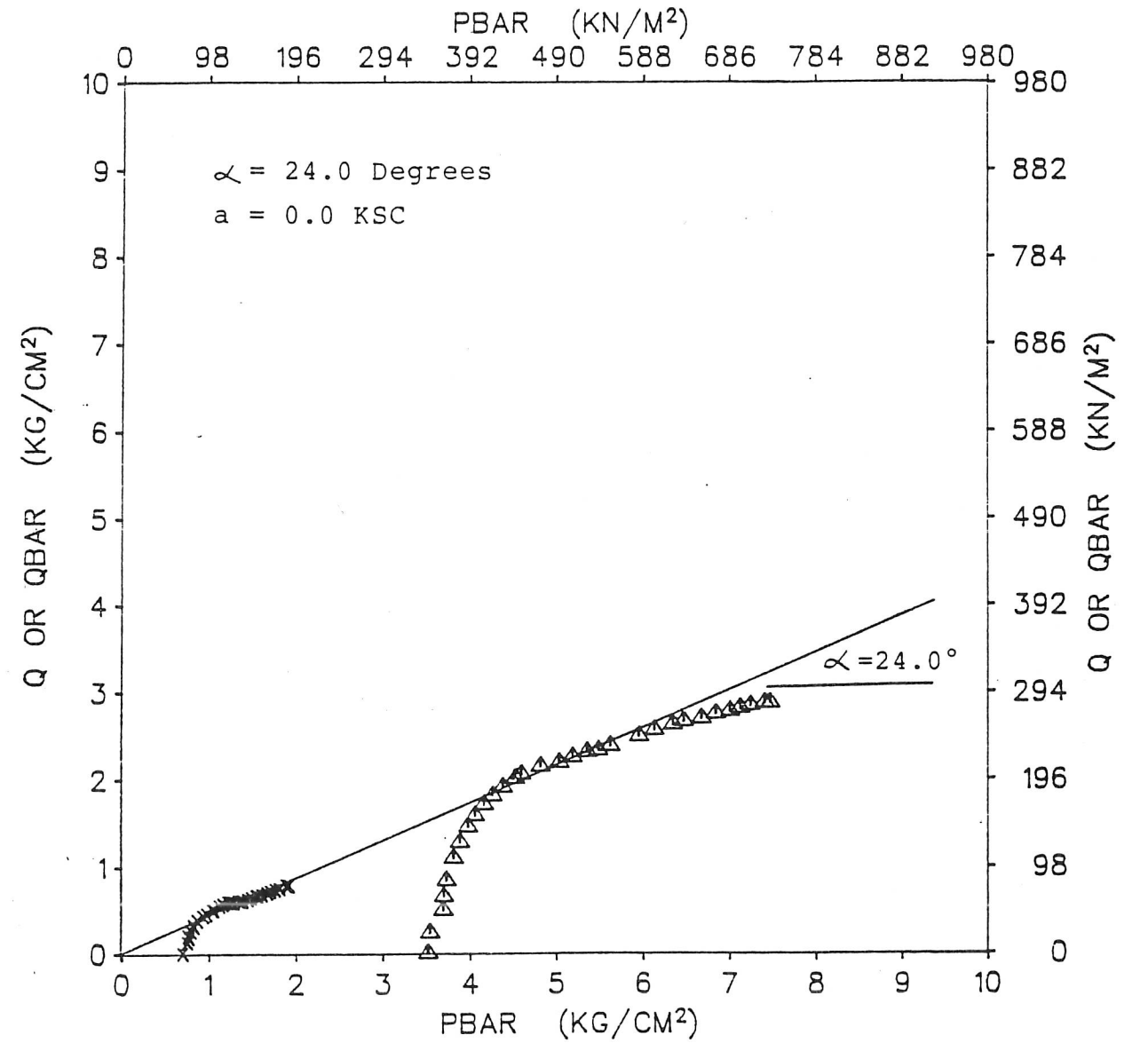
STS Consultants Ltd.

STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

|            |         |              |
|------------|---------|--------------|
| Boring: S5 | Sample: | Depth: 45-46 |
| Boring: S5 | Sample: | Depth: 46-47 |

STRESS PATH PLOT



$\times$   $\sigma_3 = 0.7$  ksc  
 $\Delta$   $\sigma_3 = 3.5$  ksc

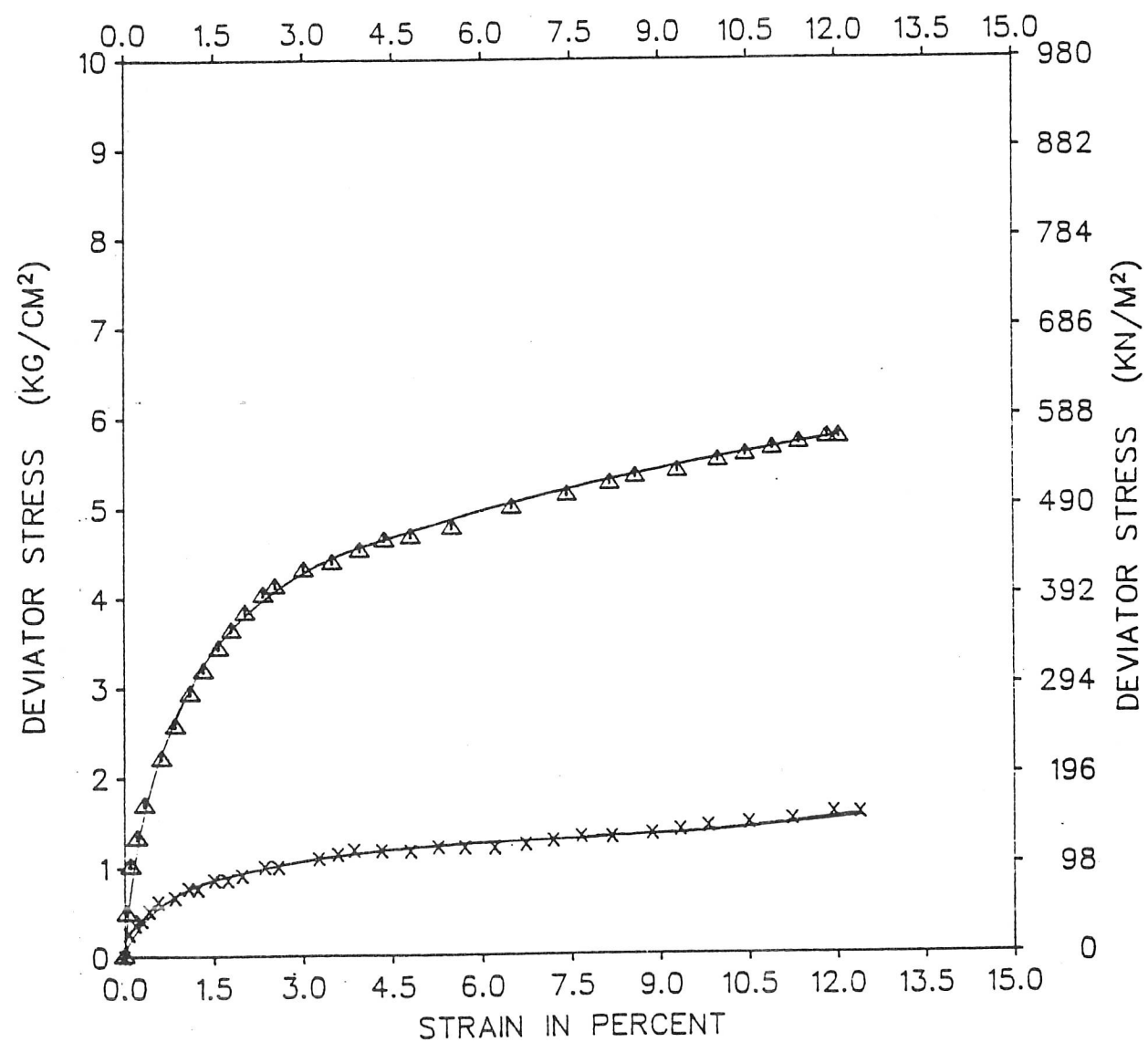
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STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

Boring: S5      Sample:      Depth: 45-46  
 Boring: S5      Sample:      Depth: 46-47

DEVIATOR STRESS vs STRAIN



x  $\sigma_3 = 0.7$  ksc  
 Δ  $\sigma_3 = 3.5$  ksc

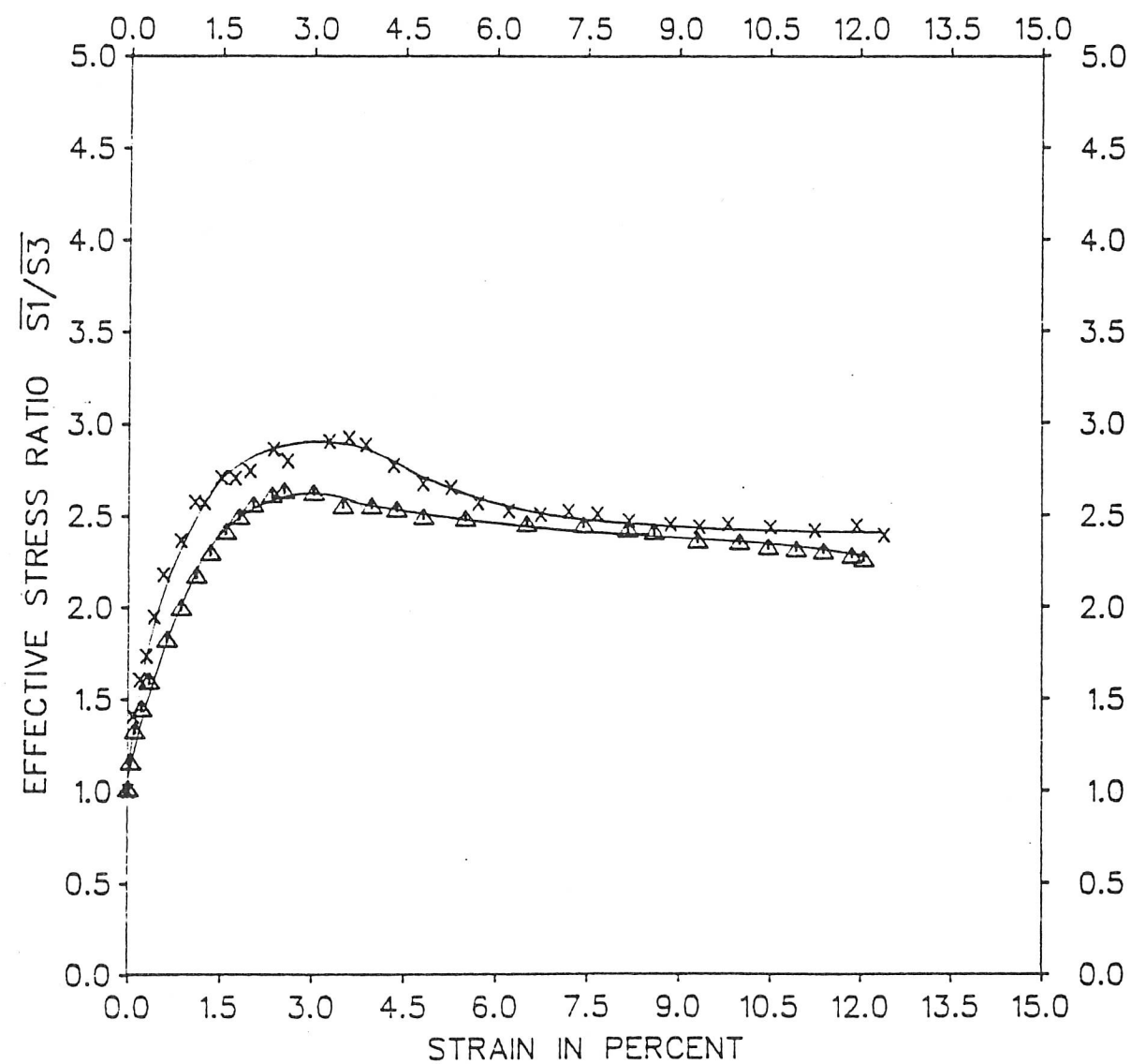
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STS JOB NO. 25331

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

Boring: S5      Sample:      Depth: 45-46  
 Boring: S5      Sample:      Depth: 46-47

EFFECTIVE STRESS RATIO vs STRAIN



x  $\sigma_3 = 0.7$  ksc  
 Δ  $\sigma_3 = 3.5$  ksc

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CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

Boring: S5

Sample:

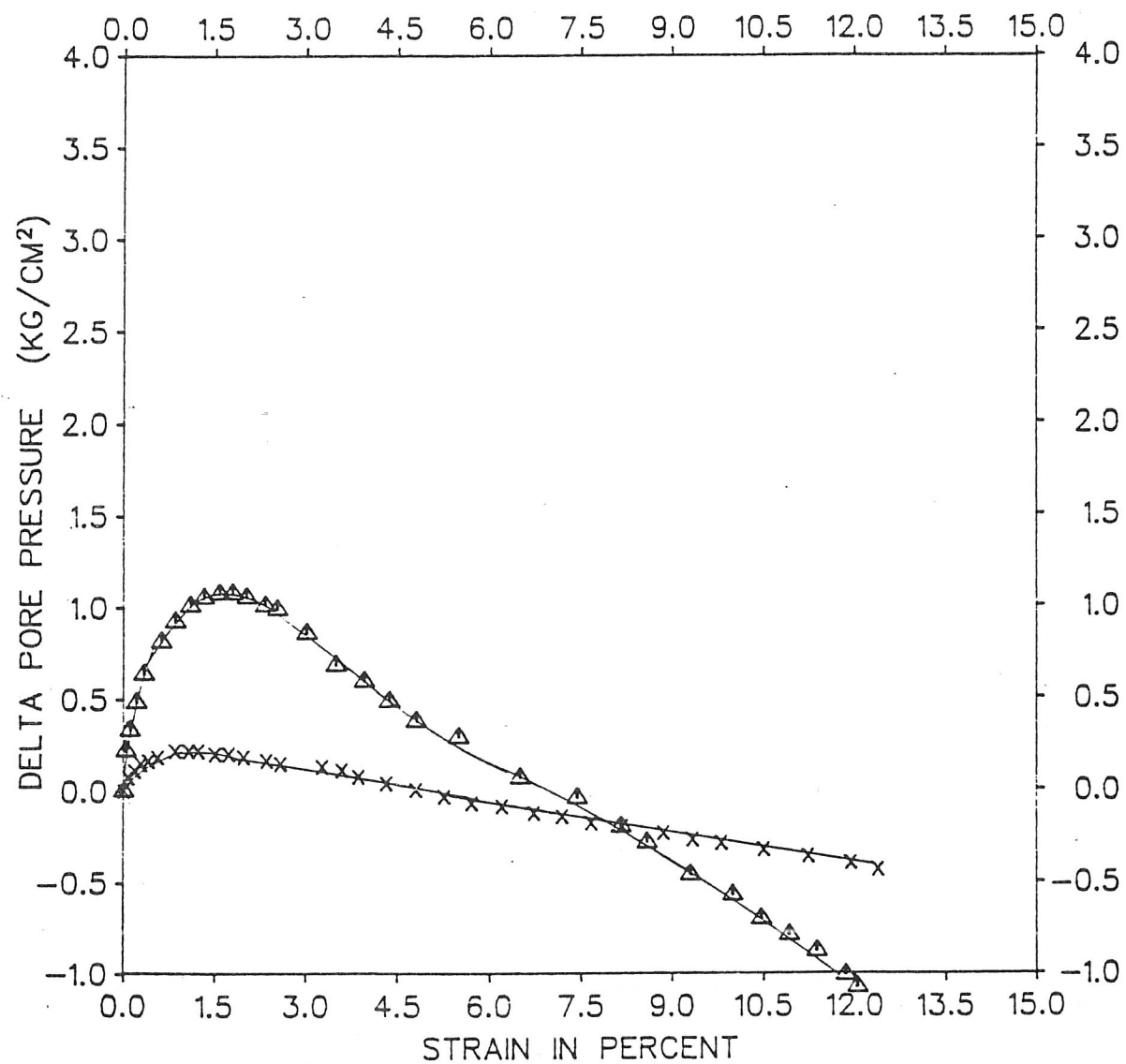
Depth: 45-46

Boring: S5

Sample:

Depth: 46-47

DELTA PORE PRESSURE vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 3.5 ksc

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CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

Boring: S5

Sample:

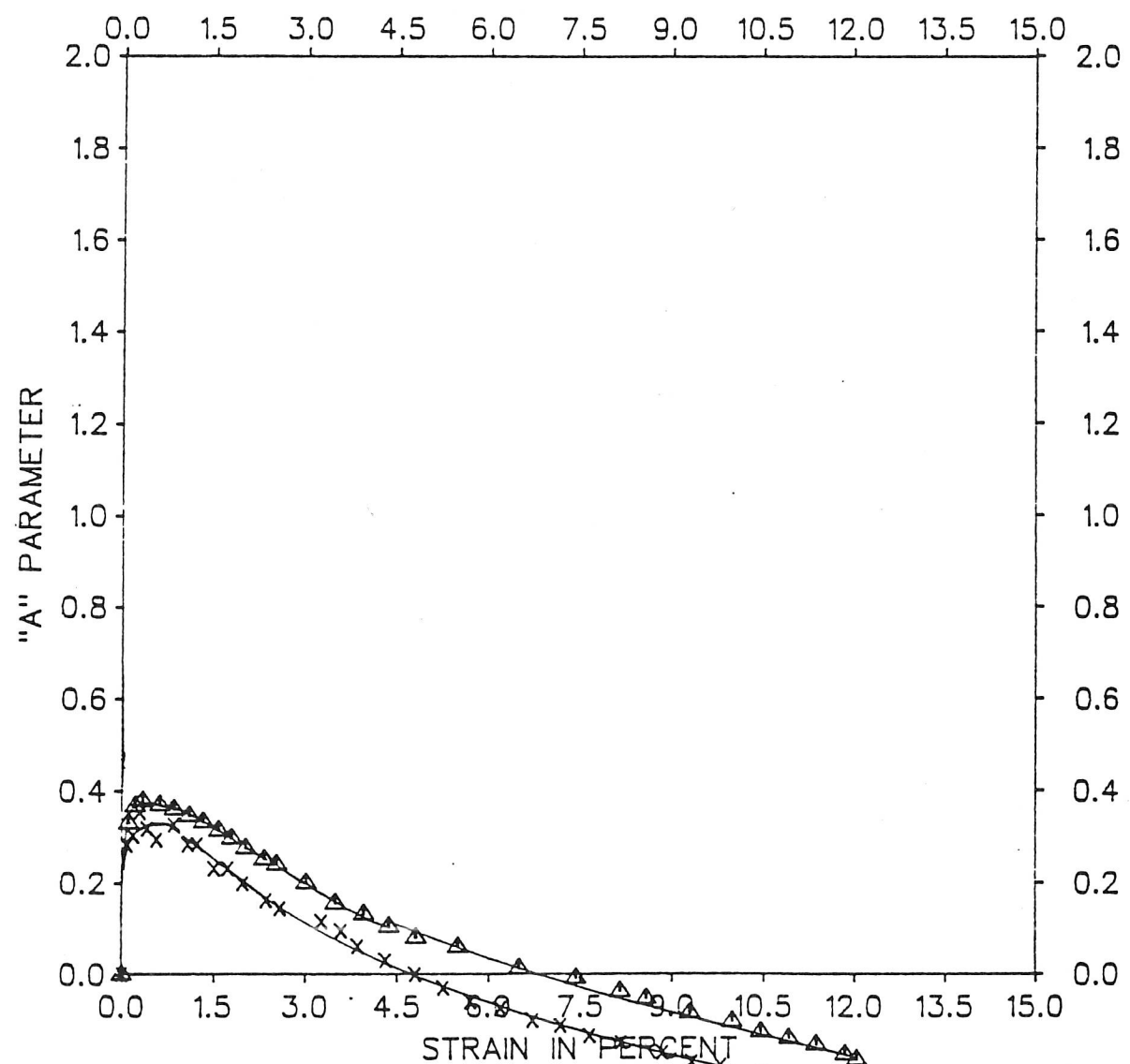
Depth: 45-46

Boring: S5

Sample:

Depth: 46-47

"A" PARAMETER vs STRAIN



x Sigma 3 = 0.7 ksc  
 Δ Sigma 3 = 3.5 ksc

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STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
BORING: S5  
SAMPLE:  
DEPTH: 45-46  
SOIL DESC: SILT TRACE CLAY TRACE FINE SAND  
-- BROWN & VERY LT. REDDISH CREAM  
(ML)  
SPEC PREP: ENDS TRIMMED

STS JOB NO: 25331  
DATE: 3-7-88  
TESTED BY: JJ  
APPROVED BY: LPO

BORING: S5  
SAMPLE:  
DEPTH: 45-46

STS JOB NO: 25331  
EFF. SIGMA3: 0.700 KG/CM2

| SPECIMEN CHARACTERISTICS----- |       | INITIAL | CONSOLIDATED |
|-------------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE              | MM    | 62.070  | 61.634       |
| LENGTH---AVERAGE              | MM    | 132.000 | 131.060      |
| AREA                          | CM2   | 30.259  | 29.835       |
| VOLUME                        | CM3   | 399.418 | 391.017      |
| WET DENSITY                   | G/CM3 | 2.224   | 2.320        |
| DRY DENSITY                   | G/CM3 | 1.958   | 2.000        |
| WATER CONTENT                 | %     | 13.600  | 16.000       |

| TEST PARAMETERS FOR CONSOLIDATION----- |        |       |
|--|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE           | KG/CM2 | 4.700 |
| TOTAL SIGMA3 + BACK PRESSURE           | KG/CM2 | 4.700 |
| BACK PRESSURE                          | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                      | KG/CM2 | 0.700 |
| EFFECTIVE SIGMA 3                      | KG/CM2 | 0.700 |
| CONSOLIDATION RATIO                    |        | 1.000 |
| STRAIN RATE                            | MM/MIN | 0.100 |

| LOAD | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | S1 - | S1BAR/ | P      | PBAR   | Q OR   | A      |
|------|-------|-------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| KG   | MM    | MM2   | P.W.P. | TOTAL  | TOTAL  | BAR    | BAR    | %      | S3   | S3BAR  | KG/CM2 | KG/CM2 | KG/CM2 | KG/CM2 |
| 0.0  | 0.00  | 2983. | 0.00   | 0.70   | 0.70   | 0.70   | 0.70   | 0.0    | 0.00 | 1.00   | 0.70   | 0.70   | 0.00   | 0.00   |
| 7.6  | 0.10  | 2986. | 0.07   | 0.95   | 0.70   | 0.88   | 0.63   | 0.1    | 0.25 | 1.41   | 0.83   | 0.76   | 0.13   | 0.28   |
| 10.7 | 0.24  | 2989. | 0.11   | 1.06   | 0.70   | 0.95   | 0.59   | 0.2    | 0.36 | 1.60   | 0.88   | 0.77   | 0.18   | 0.30   |
| 12.2 | 0.38  | 2992. | 0.14   | 1.11   | 0.70   | 0.96   | 0.56   | 0.3    | 0.41 | 1.73   | 0.90   | 0.76   | 0.20   | 0.35   |
| 15.3 | 0.54  | 2996. | 0.16   | 1.21   | 0.70   | 1.05   | 0.54   | 0.4    | 0.51 | 1.95   | 0.96   | 0.79   | 0.26   | 0.32   |
| 18.4 | 0.74  | 3000. | 0.18   | 1.31   | 0.70   | 1.13   | 0.52   | 0.6    | 0.61 | 2.18   | 1.01   | 0.83   | 0.31   | 0.29   |
| 19.9 | 1.11  | 3009. | 0.22   | 1.36   | 0.70   | 1.15   | 0.48   | 0.8    | 0.66 | 2.37   | 1.03   | 0.81   | 0.33   | 0.33   |
| 23.0 | 1.41  | 3016. | 0.22   | 1.46   | 0.70   | 1.25   | 0.48   | 1.1    | 0.76 | 2.58   | 1.08   | 0.87   | 0.38   | 0.28   |
| 23.0 | 1.61  | 3021. | 0.22   | 1.46   | 0.70   | 1.24   | 0.48   | 1.2    | 0.76 | 2.57   | 1.08   | 0.86   | 0.38   | 0.28   |
| 26.0 | 1.97  | 3029. | 0.20   | 1.56   | 0.70   | 1.36   | 0.50   | 1.5    | 0.86 | 2.71   | 1.13   | 0.93   | 0.43   | 0.23   |
| 26.0 | 2.27  | 3036. | 0.20   | 1.56   | 0.70   | 1.36   | 0.50   | 1.7    | 0.86 | 2.71   | 1.13   | 0.93   | 0.43   | 0.23   |
| 27.6 | 2.59  | 3044. | 0.18   | 1.61   | 0.70   | 1.43   | 0.52   | 2.0    | 0.91 | 2.74   | 1.15   | 0.97   | 0.45   | 0.20   |
| 30.6 | 3.09  | 3056. | 0.16   | 1.70   | 0.70   | 1.54   | 0.54   | 2.4    | 1.00 | 2.86   | 1.20   | 1.04   | 0.50   | 0.16   |
| 30.6 | 3.39  | 3063. | 0.14   | 1.70   | 0.70   | 1.56   | 0.56   | 2.6    | 1.00 | 2.80   | 1.20   | 1.06   | 0.50   | 0.14   |
| 33.7 | 4.28  | 3084. | 0.13   | 1.79   | 0.70   | 1.67   | 0.57   | 3.3    | 1.09 | 2.90   | 1.25   | 1.12   | 0.55   | 0.12   |
| 35.2 | 4.70  | 3094. | 0.11   | 1.84   | 0.70   | 1.73   | 0.59   | 3.6    | 1.14 | 2.92   | 1.27   | 1.16   | 0.57   | 0.09   |
| 36.7 | 5.06  | 3103. | 0.07   | 1.88   | 0.70   | 1.81   | 0.63   | 3.9    | 1.18 | 2.88   | 1.29   | 1.22   | 0.59   | 0.06   |
| 36.7 | 5.66  | 3118. | 0.04   | 1.88   | 0.70   | 1.84   | 0.66   | 4.3    | 1.18 | 2.77   | 1.29   | 1.25   | 0.59   | 0.03   |
| 36.7 | 6.29  | 3134. | 0.00   | 1.87   | 0.70   | 1.87   | 0.70   | 4.8    | 1.17 | 2.67   | 1.29   | 1.29   | 0.59   | 0.00   |
| 38.3 | 6.89  | 3149. | -0.04  | 1.92   | 0.70   | 1.95   | 0.74   | 5.3    | 1.22 | 2.65   | 1.31   | 1.34   | 0.61   | -0.03  |
| 38.3 | 7.47  | 3164. | -0.07  | 1.91   | 0.70   | 1.98   | 0.77   | 5.7    | 1.21 | 2.57   | 1.31   | 1.38   | 0.61   | -0.06  |
| 38.3 | 8.13  | 3181. | -0.09  | 1.90   | 0.70   | 1.99   | 0.79   | 6.2    | 1.20 | 2.53   | 1.30   | 1.39   | 0.60   | -0.07  |
| 39.8 | 8.82  | 3199. | -0.13  | 1.94   | 0.70   | 2.07   | 0.82   | 6.7    | 1.24 | 2.51   | 1.32   | 1.45   | 0.62   | -0.10  |
| 41.3 | 9.42  | 3215. | -0.14  | 1.98   | 0.70   | 2.13   | 0.84   | 7.2    | 1.28 | 2.52   | 1.34   | 1.49   | 0.64   | -0.11  |
| 42.9 | 10.04 | 3231. | -0.18  | 2.03   | 0.70   | 2.21   | 0.88   | 7.7    | 1.33 | 2.51   | 1.36   | 1.54   | 0.66   | -0.13  |
| 42.9 | 10.72 | 3249. | -0.20  | 2.02   | 0.70   | 2.22   | 0.90   | 8.2    | 1.32 | 2.47   | 1.36   | 1.56   | 0.66   | -0.15  |
| 44.4 | 11.61 | 3273. | -0.23  | 2.06   | 0.70   | 2.29   | 0.93   | 8.9    | 1.36 | 2.45   | 1.38   | 1.61   | 0.68   | -0.17  |
| 45.9 | 12.23 | 3291. | -0.27  | 2.09   | 0.70   | 2.36   | 0.97   | 9.3    | 1.39 | 2.44   | 1.40   | 1.67   | 0.70   | -0.19  |
| 47.5 | 12.85 | 3308. | -0.29  | 2.14   | 0.70   | 2.42   | 0.99   | 9.8    | 1.44 | 2.45   | 1.42   | 1.70   | 0.72   | -0.20  |
| 49.0 | 13.76 | 3333. | -0.32  | 2.17   | 0.70   | 2.49   | 1.02   | 10.5   | 1.47 | 2.44   | 1.43   | 1.76   | 0.73   | -0.22  |
| 50.5 | 14.72 | 3361. | -0.36  | 2.20   | 0.70   | 2.56   | 1.06   | 11.2   | 1.50 | 2.42   | 1.45   | 1.81   | 0.75   | -0.24  |
| 53.6 | 15.64 | 3388. | -0.39  | 2.28   | 0.70   | 2.68   | 1.09   | 11.9   | 1.58 | 2.44   | 1.49   | 1.89   | 0.79   | -0.25  |
| 53.6 | 16.23 | 3405. | -0.43  | 2.27   | 0.70   | 2.71   | 1.13   | 12.4   | 1.57 | 2.39   | 1.49   | 1.92   | 0.79   | -0.27  |

STS CONSULTANTS, LTD.

TRIAxIAL COMPRESSION TEST  
CONSOLIDATED UNDRAINED - DATA

PROJECT: KENNICOTT GEOTECHNICAL  
BORING: S5  
SAMPLE:  
DEPTH: 46-47

STS JOB NO: 25331  
DATE: 3-7-88  
TESTED BY: JJ  
APPROVED BY: UPC

SOIL DESC: SILT TRACE CLAY TRACE FINE SAND  
BROWN AND VERY LT. REDDISH CREAM  
(ML)

SPEC PREP: ENDS TRIMMED

| SPECIMEN CHARACTERISTICS |       | INITIAL | CONSOLIDATED |
|--------------------------|-------|---------|--------------|
| DIAMETER-AVERAGE         | MM    | 62.070  | 59.274       |
| LENGTH---AVERAGE         | MM    | 132.650 | 130.410      |
| AREA                     | CM2   | 30.259  | 27.594       |
| VOLUME                   | CM3   | 401.384 | 359.857      |
| WET DENSITY              | G/CM3 | 2.248   | 2.521        |
| DRY DENSITY              | G/CM3 | 1.995   | 2.225        |
| WATER CONTENT            | %     | 12.700  | 13.300       |

| TEST PARAMETERS FOR CONSOLIDATION |        |       |
|-----------------------------------|--------|-------|
| TOTAL SIGMA1 + BACK PRESSURE      | KG/CM2 | 7.520 |
| TOTAL SIGMA3 + BACK PRESSURE      | KG/CM2 | 7.520 |
| BACK PRESSURE                     | KG/CM2 | 4.000 |
| EFFECTIVE SIGMA 1                 | KG/CM2 | 3.520 |
| EFFECTIVE SIGMA 3                 | KG/CM2 | 3.520 |
| CONSOLIDATION RATIO               |        | 1.000 |
| STRAIN RATE                       | MM/MIN | 0.100 |

BORING: S5  
SAMPLE:  
DEPTH: 46-47

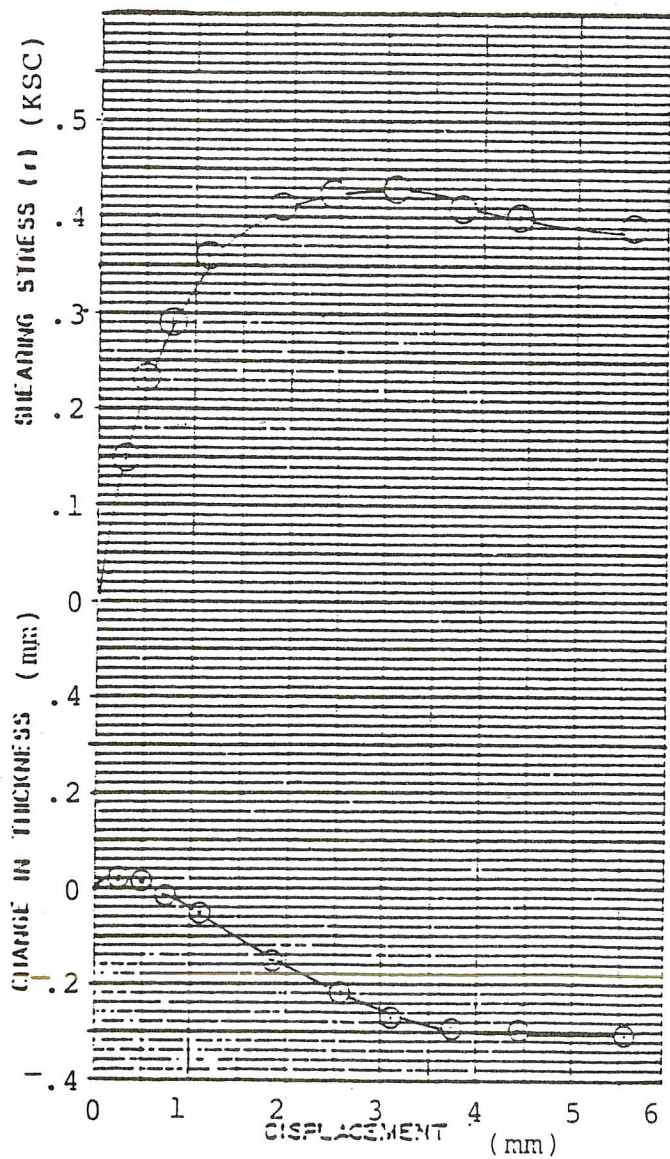
STS JOB NO: 25331  
EFF. SIGMA3: 3.520 KG/CM2

TEST RESULTS

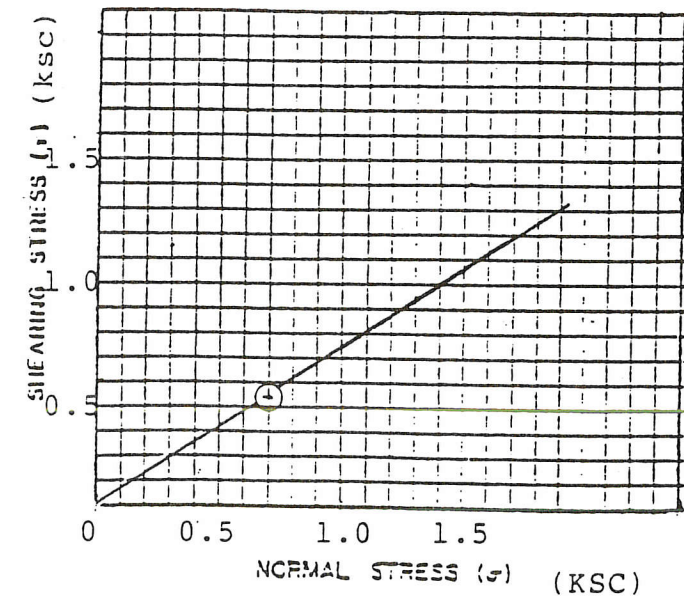
| LOAD  | DEF   | CORR  | DELTA  | SIGMA1 | SIGMA3 | SIGMA1 | SIGMA3 | STRAIN | SI - | S1BAR/ | P      | PBAR   | Q OR   | A     |
|-------|-------|-------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|-------|
| KG    | MM    | MM2   | P.W.P. | TOTAL  | TOTAL  | BAR    | BAR    | %      | S3   | S3BAR  | KG/CM2 | KG/CM2 | KG/CM2 |       |
| 0.0   | 0.00  | 2759. | 0.00   | 3.52   | 3.52   | 3.52   | 3.52   | 0.0    | 0.00 | 1.00   | 3.52   | 3.52   | 0.00   | 0.00  |
| 13.1  | 0.05  | 2760. | 0.22   | 3.99   | 3.52   | 3.78   | 3.30   | 0.0    | 0.47 | 1.14   | 3.76   | 3.54   | 0.24   | 0.46  |
| 27.6  | 0.14  | 2762. | 0.33   | 4.52   | 3.52   | 4.19   | 3.19   | 0.1    | 1.00 | 1.31   | 4.02   | 3.69   | 0.50   | 0.33  |
| 36.4  | 0.28  | 2765. | 0.48   | 4.84   | 3.52   | 4.35   | 3.04   | 0.2    | 1.32 | 1.43   | 4.18   | 3.70   | 0.66   | 0.37  |
| 46.6  | 0.44  | 2769. | 0.64   | 5.20   | 3.52   | 4.57   | 2.88   | 0.3    | 1.68 | 1.58   | 4.36   | 3.73   | 0.84   | 0.38  |
| 61.1  | 0.81  | 2777. | 0.81   | 5.72   | 3.52   | 4.91   | 2.71   | 0.6    | 2.20 | 1.81   | 4.62   | 3.81   | 1.10   | 0.37  |
| 71.3  | 1.11  | 2783. | 0.92   | 6.08   | 3.52   | 5.16   | 2.60   | 0.9    | 2.56 | 1.99   | 4.80   | 3.88   | 1.28   | 0.36  |
| 81.5  | 1.43  | 2790. | 1.01   | 6.44   | 3.52   | 5.43   | 2.51   | 1.1    | 2.92 | 2.16   | 4.98   | 3.97   | 1.46   | 0.35  |
| 88.8  | 1.73  | 2797. | 1.05   | 6.70   | 3.52   | 5.64   | 2.47   | 1.3    | 3.18 | 2.29   | 5.11   | 4.06   | 1.59   | 0.33  |
| 96.1  | 2.06  | 2804. | 1.07   | 6.95   | 3.52   | 5.87   | 2.45   | 1.6    | 3.43 | 2.40   | 5.23   | 4.16   | 1.71   | 0.31  |
| 101.3 | 2.34  | 2810. | 1.07   | 7.15   | 3.52   | 6.07   | 2.45   | 1.8    | 3.63 | 2.48   | 5.33   | 4.26   | 1.81   | 0.30  |
| 107.7 | 2.64  | 2816. | 1.05   | 7.34   | 3.52   | 6.29   | 2.47   | 2.0    | 3.82 | 2.55   | 5.43   | 4.38   | 1.91   | 0.28  |
| 113.6 | 3.04  | 2825. | 1.01   | 7.54   | 3.52   | 6.53   | 2.51   | 2.3    | 4.02 | 2.60   | 5.53   | 4.52   | 2.01   | 0.25  |
| 116.5 | 3.30  | 2831. | 0.99   | 7.64   | 3.52   | 6.65   | 2.53   | 2.5    | 4.12 | 2.62   | 5.58   | 4.59   | 2.06   | 0.24  |
| 122.3 | 3.93  | 2845. | 0.86   | 7.82   | 3.52   | 6.96   | 2.66   | 3.0    | 4.30 | 2.61   | 5.67   | 4.81   | 2.15   | 0.20  |
| 125.2 | 4.55  | 2859. | 0.68   | 7.90   | 3.52   | 7.22   | 2.84   | 3.5    | 4.38 | 2.54   | 5.71   | 5.03   | 2.19   | 0.16  |
| 129.6 | 5.16  | 2873. | 0.59   | 8.03   | 3.52   | 7.44   | 2.93   | 4.0    | 4.51 | 2.54   | 5.78   | 5.18   | 2.26   | 0.13  |
| 133.5 | 5.70  | 2886. | 0.48   | 8.15   | 3.52   | 7.66   | 3.04   | 4.4    | 4.63 | 2.52   | 5.83   | 5.35   | 2.31   | 0.10  |
| 135.2 | 6.27  | 2899. | 0.37   | 8.18   | 3.52   | 7.81   | 3.15   | 4.8    | 4.66 | 2.48   | 5.85   | 5.48   | 2.33   | 0.08  |
| 139.1 | 7.16  | 2920. | 0.29   | 8.28   | 3.52   | 8.00   | 3.23   | 5.5    | 4.76 | 2.47   | 5.90   | 5.62   | 2.38   | 0.06  |
| 147.2 | 8.48  | 2951. | 0.07   | 8.51   | 3.52   | 8.44   | 3.45   | 6.5    | 4.99 | 2.44   | 6.01   | 5.95   | 2.49   | 0.01  |
| 152.8 | 9.69  | 2981. | -0.04  | 8.65   | 3.52   | 8.69   | 3.56   | 7.4    | 5.13 | 2.44   | 6.08   | 6.13   | 2.56   | -0.01 |
| 157.8 | 10.64 | 3005. | -0.20  | 8.77   | 3.52   | 8.97   | 3.72   | 8.2    | 5.25 | 2.41   | 6.15   | 6.34   | 2.63   | -0.04 |
| 160.8 | 11.20 | 3019. | -0.29  | 8.85   | 3.52   | 9.13   | 3.81   | 8.6    | 5.33 | 2.40   | 6.18   | 6.47   | 2.66   | -0.05 |
| 163.9 | 12.13 | 3042. | -0.46  | 8.91   | 3.52   | 9.37   | 3.98   | 9.3    | 5.39 | 2.35   | 6.21   | 6.67   | 2.69   | -0.09 |
| 168.6 | 13.03 | 3066. | -0.57  | 9.02   | 3.52   | 9.59   | 4.09   | 10.0   | 5.50 | 2.34   | 6.27   | 6.84   | 2.75   | -0.10 |
| 171.4 | 13.64 | 3082. | -0.70  | 9.08   | 3.52   | 9.78   | 4.22   | 10.5   | 5.56 | 2.32   | 6.30   | 7.00   | 2.78   | -0.13 |
| 174.3 | 14.24 | 3098. | -0.79  | 9.15   | 3.52   | 9.94   | 4.31   | 10.9   | 5.63 | 2.31   | 6.33   | 7.12   | 2.81   | -0.14 |
| 177.1 | 14.83 | 3113. | -0.88  | 9.21   | 3.52   | 10.09  | 4.40   | 11.4   | 5.69 | 2.29   | 6.36   | 7.24   | 2.84   | -0.15 |
| 180.0 | 15.45 | 3130. | -1.01  | 9.27   | 3.52   | 10.28  | 4.53   | 11.8   | 5.75 | 2.27   | 6.40   | 7.40   | 2.88   | -0.18 |
| 180.4 | 15.71 | 3137. | -1.07  | 9.27   | 3.52   | 10.35  | 4.59   | 12.0   | 5.75 | 2.25   | 6.40   | 7.47   | 2.88   | -0.19 |

# DIRECT SHEAR TEST

|   |                                 |                        |                 |
|---|---------------------------------|------------------------|-----------------|
| PROJECT<br>Kenicott Geotechnical                                    |                                 | SAMPLE LOCATION<br>--- |                 |
| FIELD SAMPLE NO.<br>S-2   | DEPTH<br>5-7'                   | STS Project No. 25331  |                 |
| TYPE OF SAMPLE<br>3" Shelby Tube                                    | TESTED AT<br>STS-Northbrook     | APPROVED BY<br>W.P.O.  | DATE<br>3/11/88 |
| CLASSIFICATION<br>Silty sand, little fine gravel--reddish brown(sm) | LL -- PI --                     | SPECIFIC GRAVITY       |                 |
| TYPE OF TEST<br>Drained   | CONTROL<br>Strain               | $G_s(-)^{3/4}$         | --              |
| RATE OF LOADING<br>0.048mm/min                                      | MOISTURE CONDITION<br>saturated | $G_s(-)^{3/4}$         | --              |
| TYPE OF SPECIMEN<br>Round undisturbed                               | AREA<br>28.27cm <sup>2</sup>    | THICKNESS<br>2.00cm    |                 |



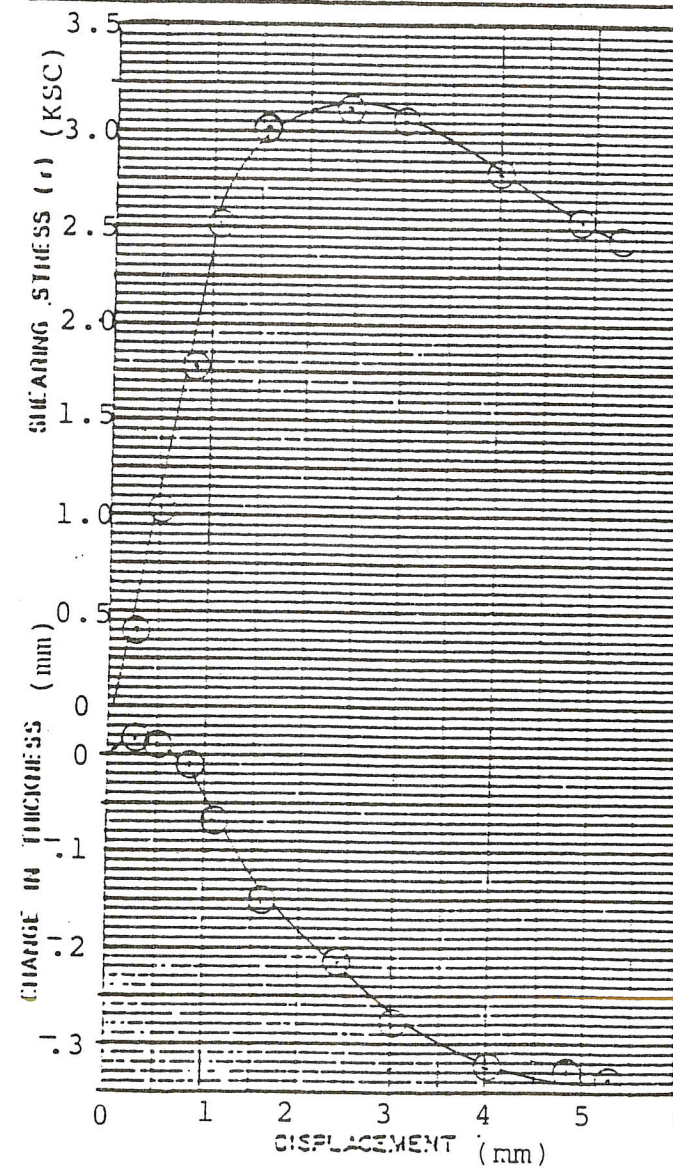
| TEST NO.                      | 1     | 2      | 3      | 4 |
|-------------------------------|-------|--------|--------|---|
| INIT MOISTURE, %              | 9.7   |        |        |   |
| DRY DENSITY, $\frac{g}{cm^3}$ | 1.987 |        |        |   |
| INIT VOID RATIO               | .349  |        |        |   |
| TEST DURATION, (min)          | 125   |        |        |   |
| FINAL MOISTURE, %             | 11.4  |        |        |   |
| NORMAL STRESS KSC             | 0.70  |        |        |   |
| MAX SHEAR STRESS KSC          | 0.41  |        |        |   |
| SHEAR VALUES                  |       |        |        |   |
|                               |       | $\phi$ | c      |   |
| AT MAXIMUM STRESS             |       |        |        |   |
|                               |       | 33°    | 0.0KSC |   |



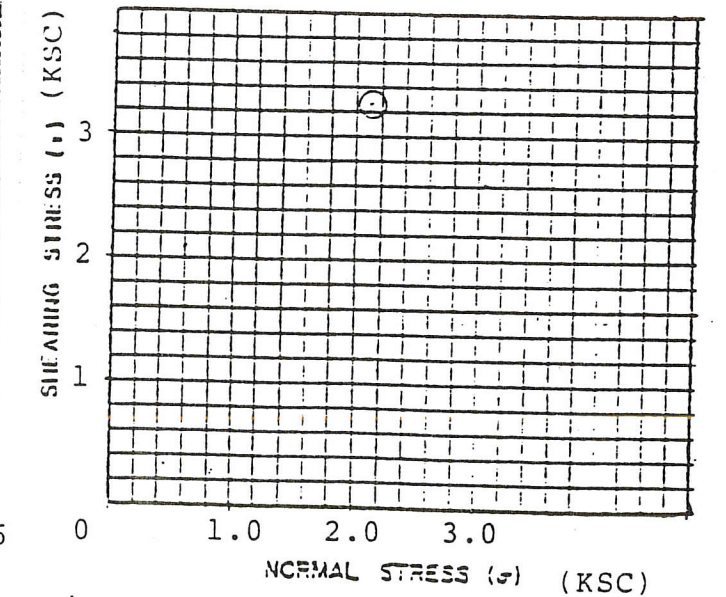
REMARKS

# DIRECT SHEAR TEST

|   |                                 |                        |                 |
|---|---------------------------------|------------------------|-----------------|
| PROJECT<br>Kenicott Geotechnical            |                                 | SAMPLE LOCATION<br>--- |                 |
| FIELD SAMPLE NO.<br>S-4                     | DEPTH<br>31.5-32.5'             | STS Project No.: 25331 |                 |
| TYPE OF SAMPLE<br>3" Shelby Tube            | TESTED AT<br>STS-northbrook     | APPROVED BY<br>W.P.O.  | DATE<br>3/11/88 |
| CLASSIFICATION<br>Fine sandy silt--tan (ML) | LL -- PI --                     | SPECIFIC GRAVITY       |                 |
| TYPE OF TEST<br>Drained                     | CONTROL<br>Strain               | $G_s(-)^{3/4}$         | --              |
| RATE OF LOADING<br>0.024mm/min              | MOISTURE CONDITION<br>saturated | $G_s(-)^{3/4}$         | --              |
| TYPE OF SPECIMEN<br>round undisturbed       | AREA<br>28.27cm <sup>2</sup>    | THICKNESS<br>2.00cm    |                 |

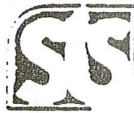


| TEST NO.                      | 1     | 2      | 3 | 4 |
|-------------------------------|-------|--------|---|---|
| INIT MOISTURE, %              | 13.0  |        |   |   |
| DRY DENSITY, $\frac{g}{cm^3}$ | 1.939 |        |   |   |
| INIT VOID RATIO               | .366  |        |   |   |
| TEST DURATION, (min)          | 250   |        |   |   |
| FINAL MOISTURE, %             | 13.8  |        |   |   |
| NORMAL STRESS KSC             | 2.11  |        |   |   |
| MAX SHEAR STRESS KSC          | 3.29  |        |   |   |
| SHEAR VALUES                  |       |        |   |   |
|                               |       | $\phi$ | c |   |
| AT MAXIMUM STRESS             |       |        |   |   |



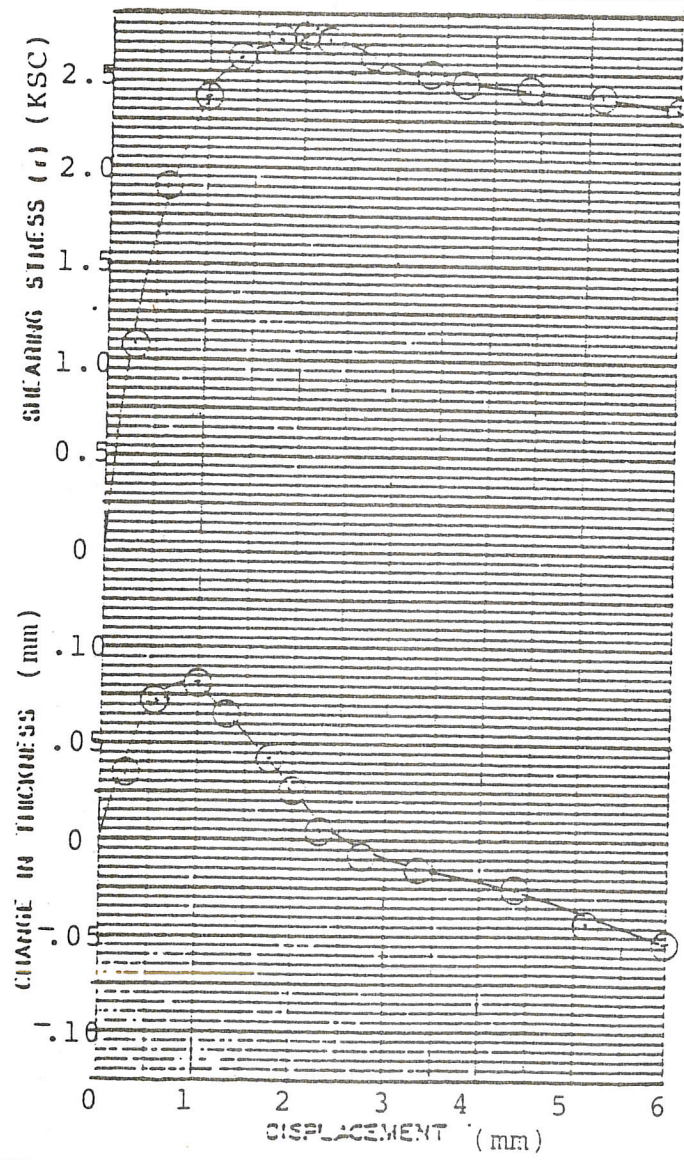
REMARKS

Note: Sample extremely hard. Require additional direct shear points to determine  $\phi$  angle.

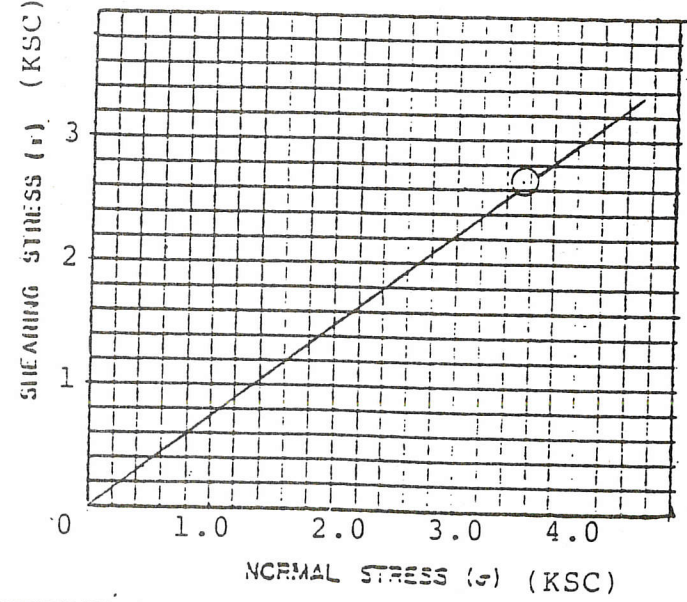


# DIRECT SHEAR TEST

|  |                              |                        |              |
|--|------------------------------|------------------------|--------------|
| PROJECT Kenicott Geotechnical          |                              | SAMPLE LOCATION ---    |              |
| FIELD SAMPLE NO. S-5                   | DEPTH 35-36'                 | STS Project No.: 25331 |              |
| TYPE OF SAMPLE 3" Shelby Tube          | TESTED AT STS-Northbrook     | APPROVED BY W.P.Q.     | DATE 3/11/88 |
| CLASSIFICATION Fine sand -- cream (SP) | LL -- PI --                  | SPECIFIC GRAVITY       |              |
| TYPE OF TEST Drained                   | CONTROL Strain               | $G_s(-) \%$            | --           |
| RATE OF LOADING 0.048mm/min            | MOISTURE CONDITION saturated | $G_s(-) \%$            | --           |
| TYPE OF SPECIMEN Round undisturbed     | AREA 28.27cm <sup>2</sup>    | THICKNESS 2.00cm       |              |



| TEST NO.                      | 1     | 2      | 3   | 4 |
|-------------------------------|-------|--------|-----|---|
| INIT MOISTURE, %              | 18.5  |        |     |   |
| DRY DENSITY, $\frac{MBS}{WT}$ | 1.823 |        |     |   |
| INIT VOID RATIO               | .438  |        |     |   |
| TEST DURATION, (min)          | 125   |        |     |   |
| FINAL MOISTURE, %             | 21.6  |        |     |   |
| NORMAL STRESS KSC             | 3.52  |        |     |   |
| MAX SHEAR STRESS KSC          | 2.69  |        |     |   |
| SHEAR VALUES                  |       |        |     |   |
|                               |       | $\phi$ | c   |   |
| AT MAXIMUM STRESS             |       | 36.5°  | 0.0 |   |



REMARKS